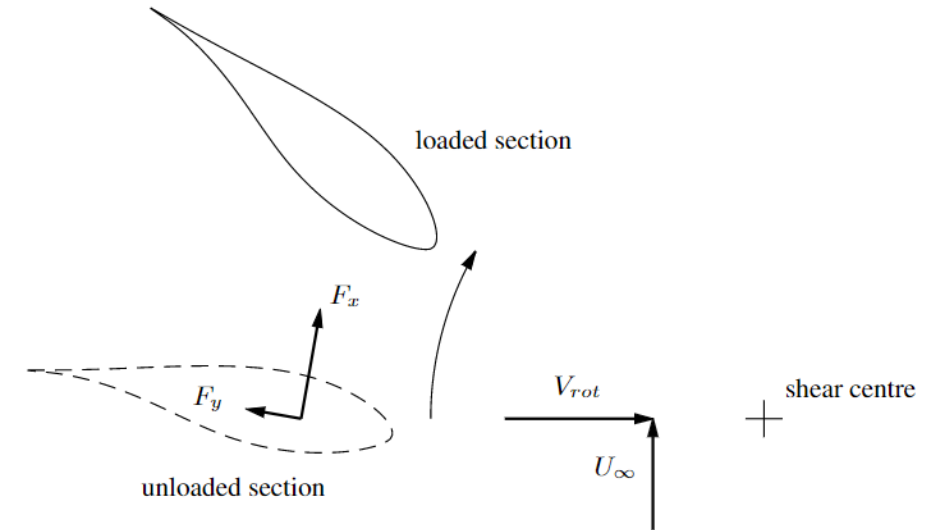


› **EXPERIMENTAL ANALYSIS OF THE EFFECT OF BLADE
SWEEP ON A SCALED IEA 15 MW WIND TURBINE**
ERIK FRITZ | ANDRÉ RIBEIRO | CARLOS FERREIRA | KOEN BOORSMA

› MOTIVATION

› Motivation for blade sweep:

- › Wind turbine blades are becoming increasingly long and flexible
- › Measures for aeroelastic tailoring are becoming important
- › Blade sweep couples bending and torsional deformations
- › Distance between aerodynamic centre and shear centre
- › Example: Aft-swept blade twists to lower angles of attack when loaded → load reduction



› Motivation for this experiment:

- › Better understand the aerodynamics of swept wind turbine blades
- › Create a dataset to validate numerical models for swept blades
- › Bonus: Create an experimental dataset of a thrust-scaled IEA 15 MW RWT model

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RESEARCH ARTICLE

WILEY

An efficient blade sweep correction model for blade element momentum theory

Erik Kaspar Fritz^{1,2} | Carlos Ferreira² | Koen Boorsma¹

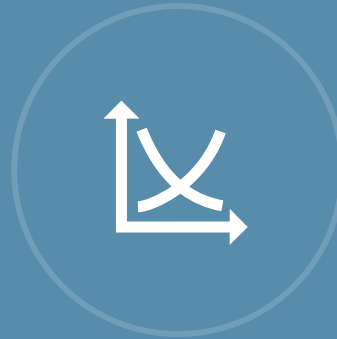
› PRESENTATION OVERVIEW



Experimental setup



Data processing



Results



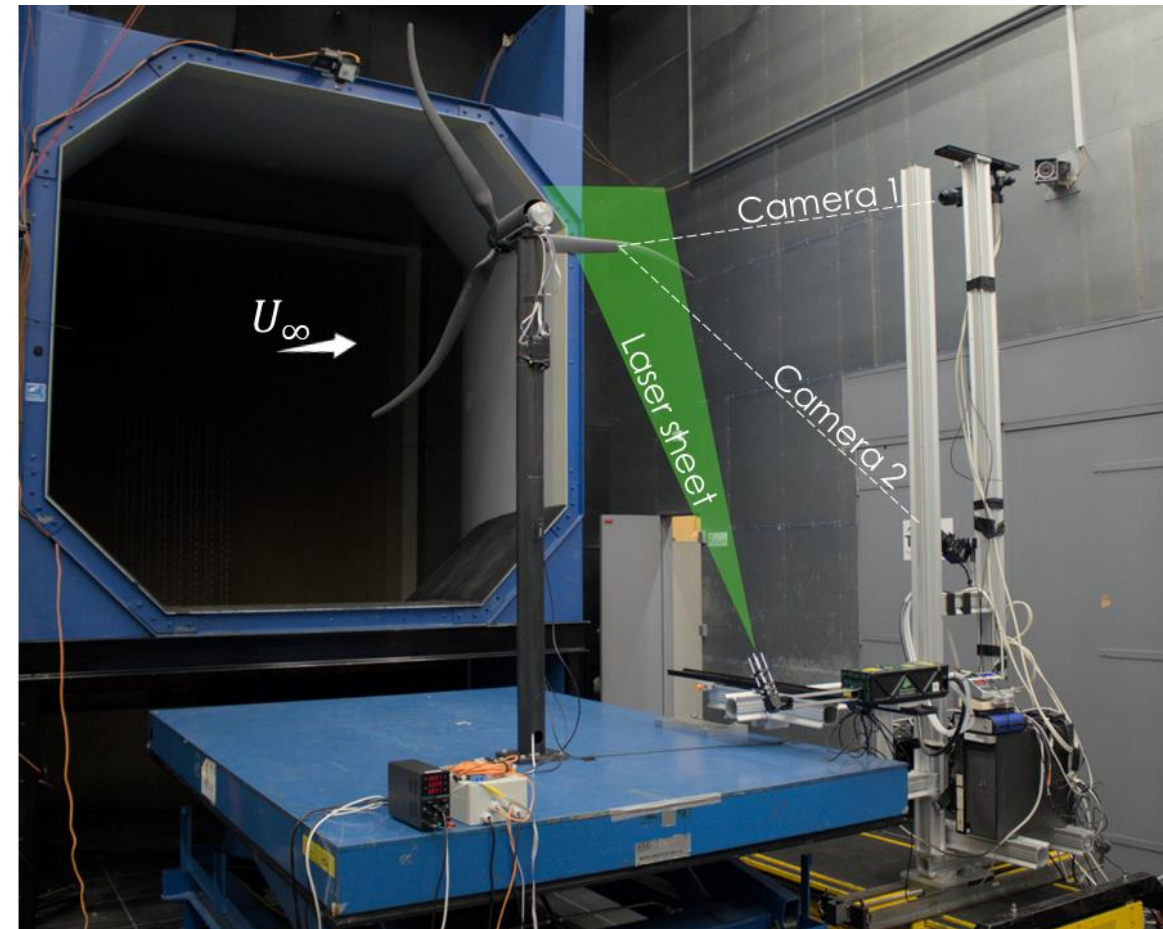
Conclusions

EXPERIMENTAL SETUP OVERVIEW

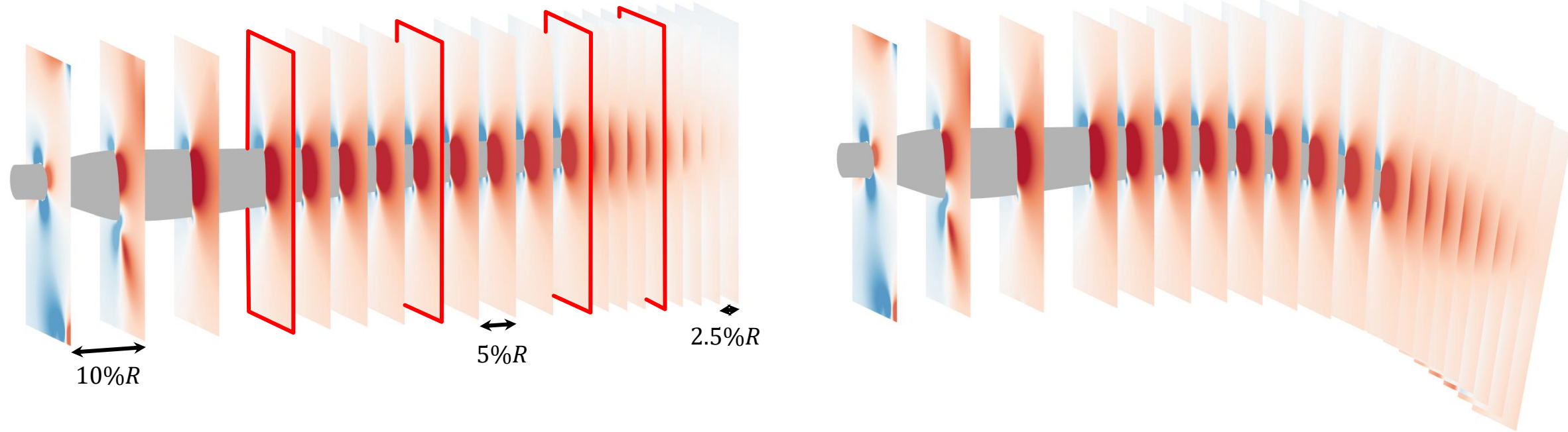
Carbon fibre-reinforced blades (vacuum-infused)



Measurement system (Particle Image Velocimetry)



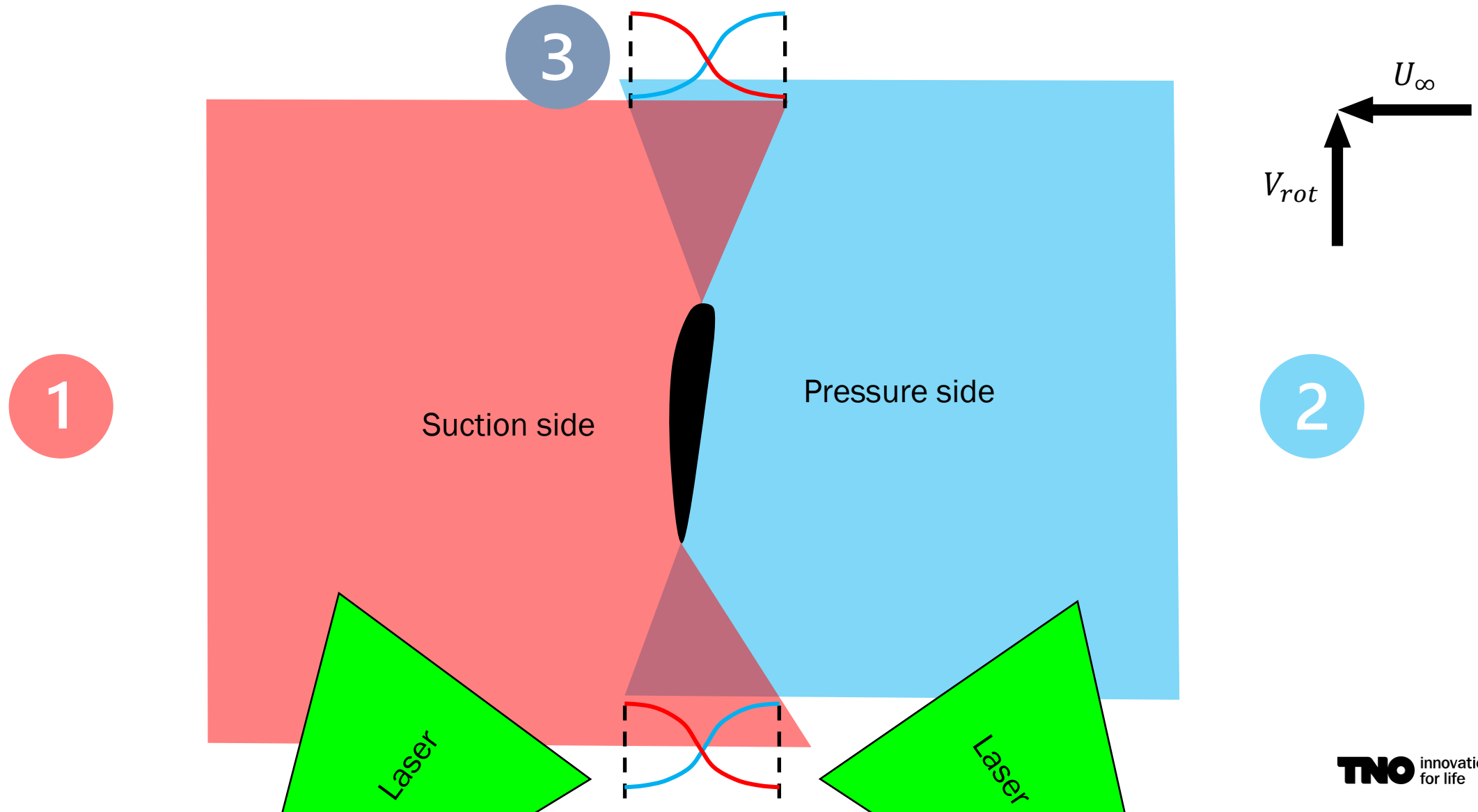
› EXPERIMENTAL SETUP MEASUREMENT PLAN



- › $U_{\infty} = 3.75 \frac{m}{s}$, $\lambda = 9$, $\beta_{pitch} = 0^{\circ}$
- › 20 planes per blade configuration, higher resolution towards the tip
- › At 40%, 60%, 80% and 90% radius, all three blades are measured, at all other locations only one blade
- › For swept blade configuration, planes are chosen at radius identical to straight blade planes

DATA PROCESSING

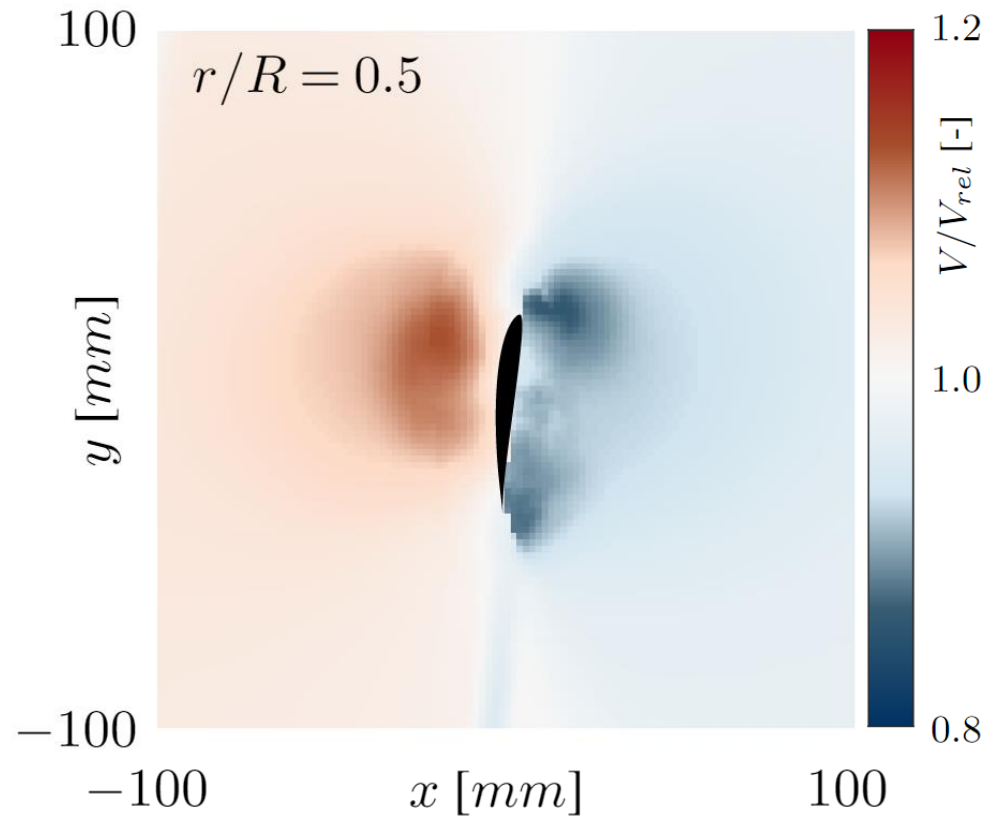
STITCHING THE PIV MEASUREMENTS



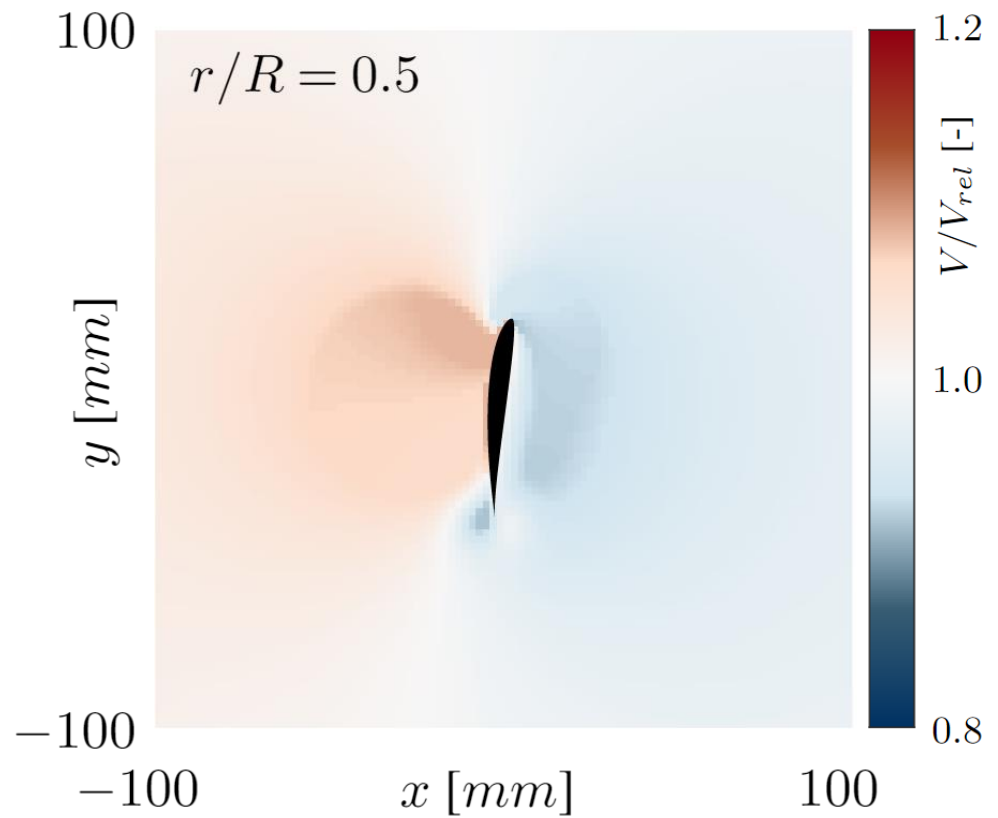
DATA PROCESSING

FLOW FIELD

› Measured flow field



› Panel code simulations for comparison



DATA PROCESSING

CIRCULATION AND FORCE DERIVATION

- › Circulation from velocity integral:

$$\Gamma = - \oint_S \mathbf{u} \cdot d\mathbf{s}$$

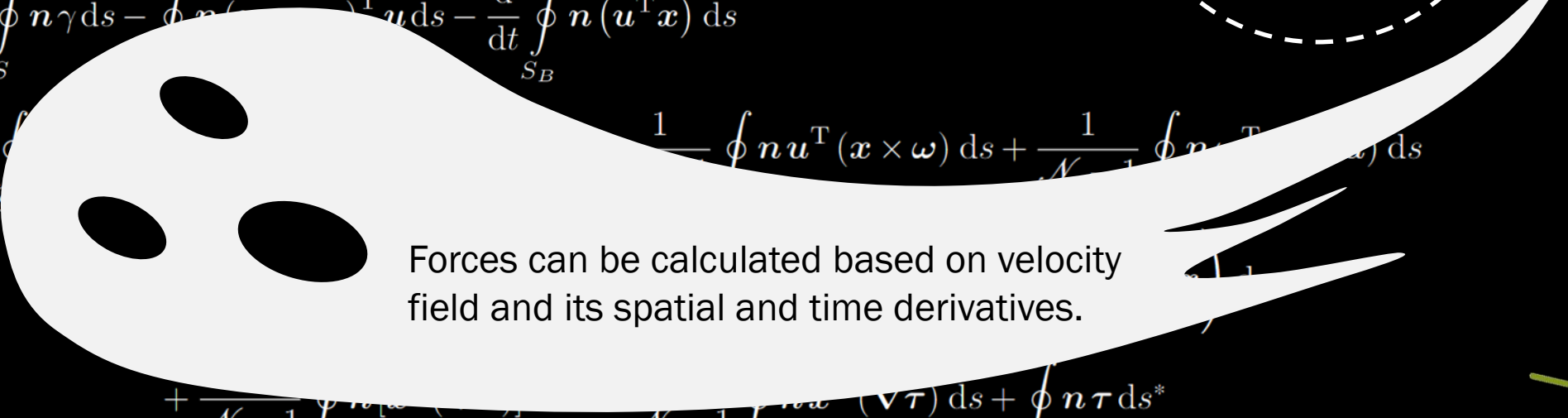
- › Forces from velocity field using Noca's method [1]:

$$\frac{\mathbf{F}}{\rho} = \oint_S \mathbf{n} \gamma ds - \oint_S \mathbf{n} (\mathbf{u}^T \mathbf{x}) ds - \frac{d}{dt} \oint_{S_B} \mathbf{n} (\mathbf{u}^T \mathbf{x}) ds$$

$$\frac{\mathbf{F}}{\rho} = \oint_S \mathbf{n} \gamma ds + \frac{1}{\mathcal{N}-1} \oint_S \mathbf{n} \mathbf{u}^T (\mathbf{x} \times \boldsymbol{\omega}) ds + \frac{1}{\mathcal{N}-1} \oint_S \mathbf{n} \mathbf{u}^T (\mathbf{x} \times \boldsymbol{\omega}) ds$$

Forces can be calculated based on velocity field and its spatial and time derivatives.

Control volume

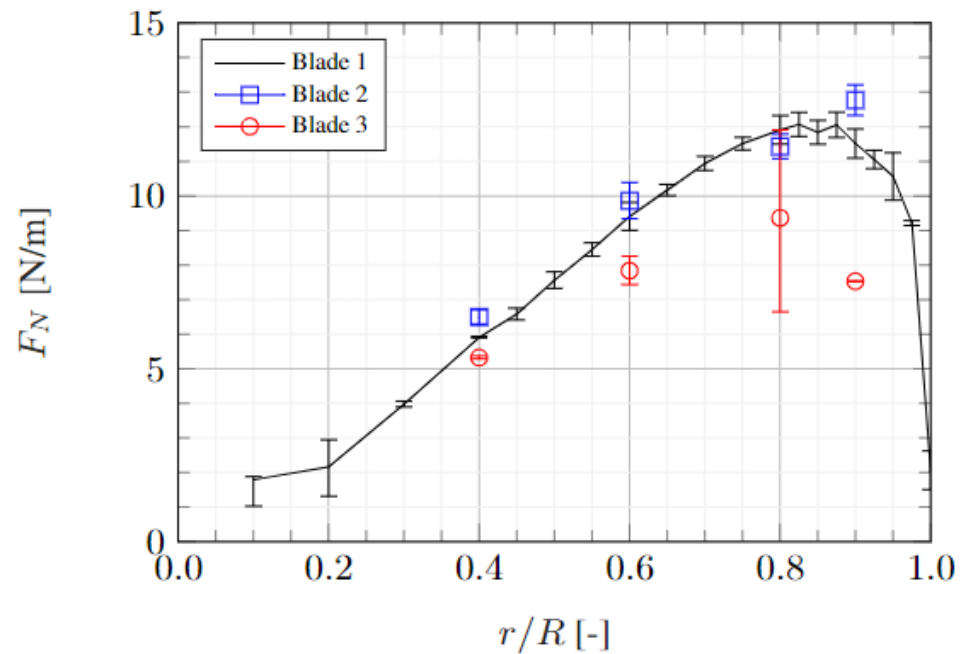
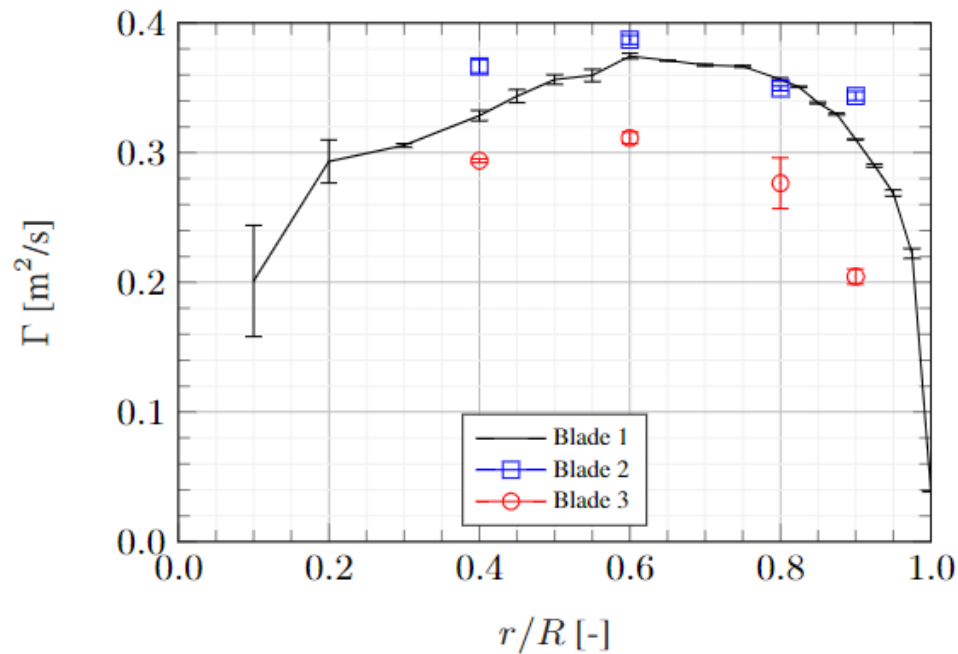


[1] Noca et al. (1999): A comparison of methods for evaluating time-dependant fluid dynamic forces on bodies, using only velocity fields and their derivatives, <https://doi.org/10.1006/jfls.1999.0219>

DATA PROCESSING

DISCREPANCIES BETWEEN BLADES

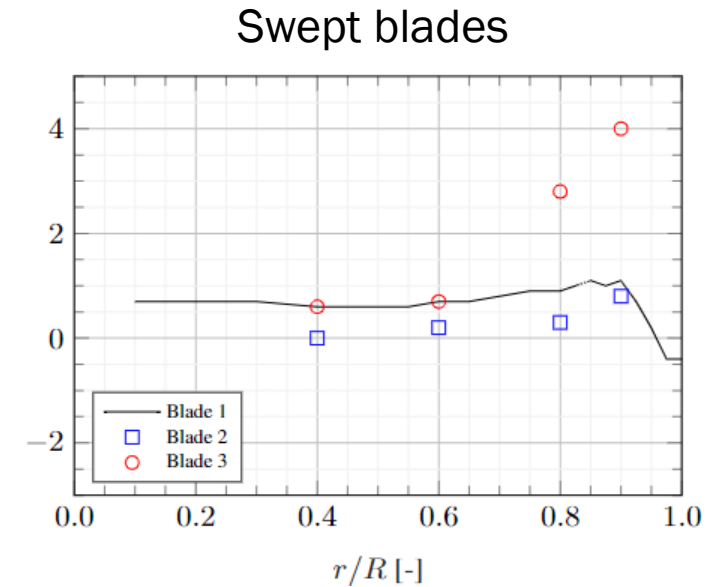
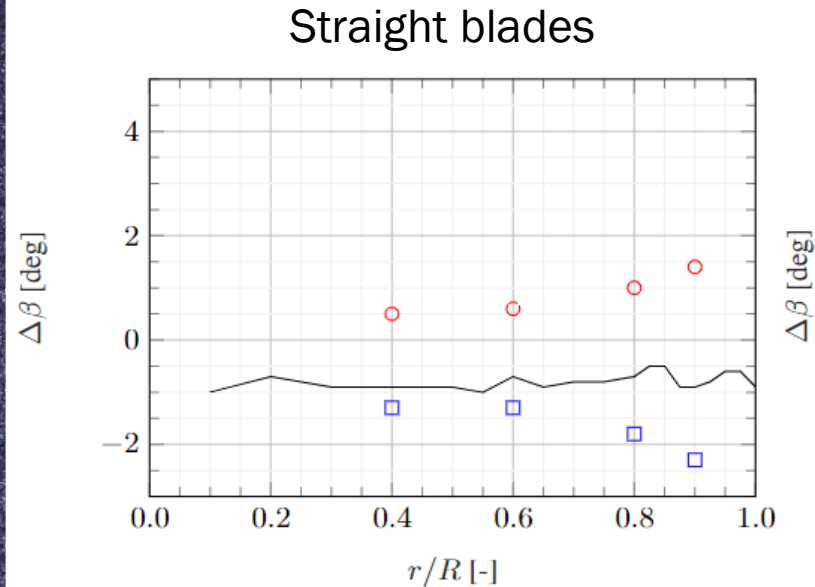
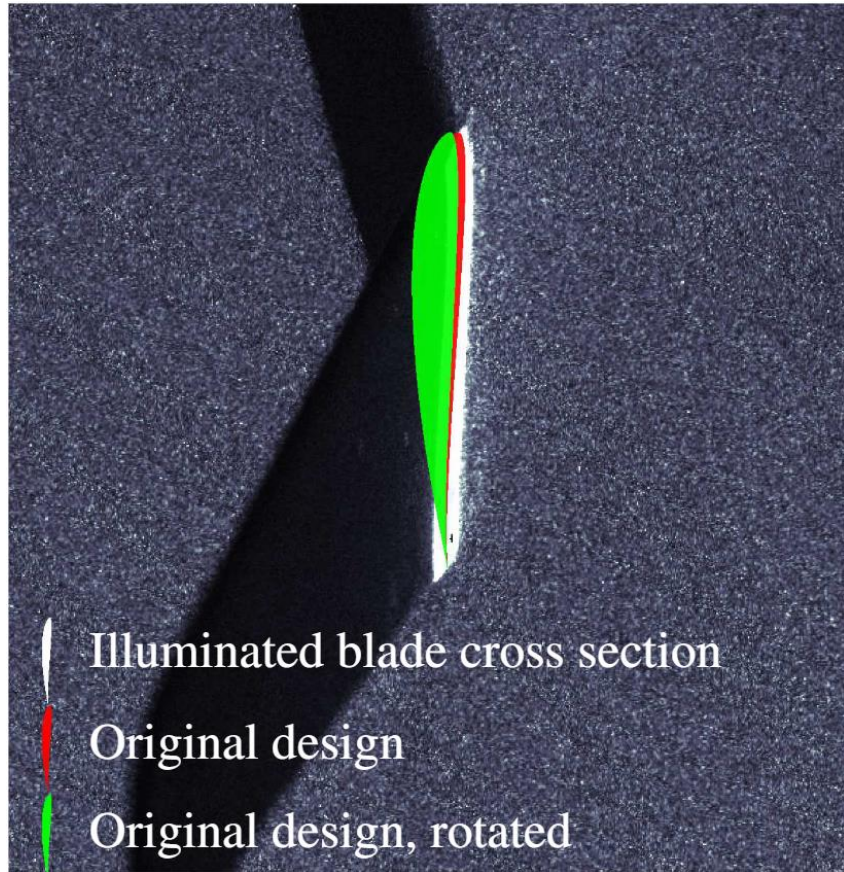
- › Large differences in aerodynamic quantities between the three blades



- › What causes these discrepancies?
- › Can we correct for this?

DATA PROCESSING

PITCH OFFSET / TWIST DEFORMATION



› Explanation:

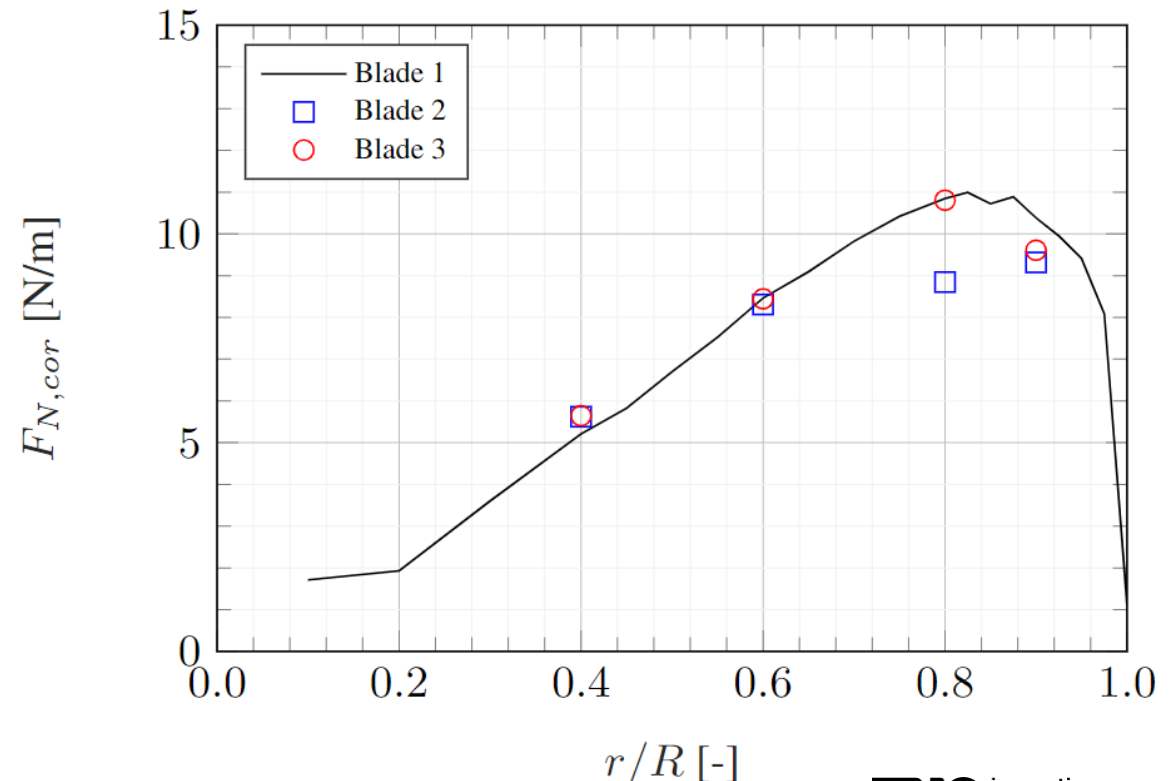
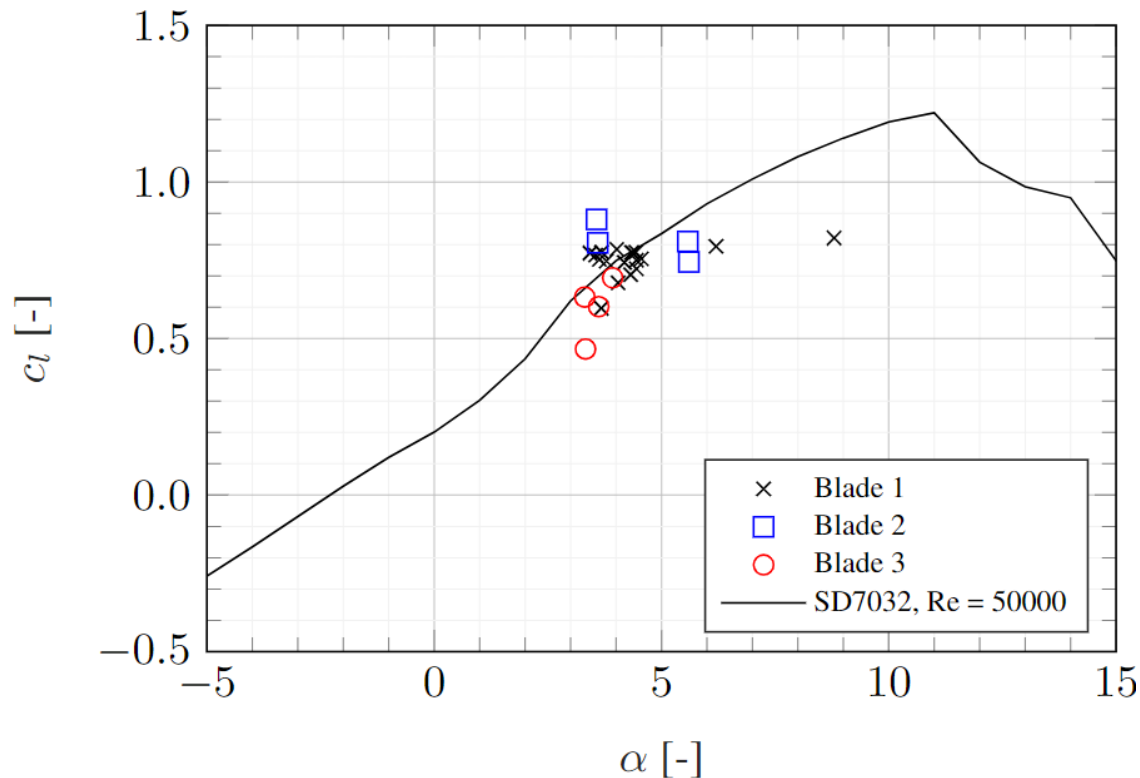
- › Manual manufacturing leading to differences in final fibre layup
- › Manual mechanism to set pitch angle

DATA PROCESSING

PITCH OFFSET / TWIST DEFORMATION - CORRECTION

› Apply inverse BEM (including twist/pitch offset) to derive values of induction and angle of attack

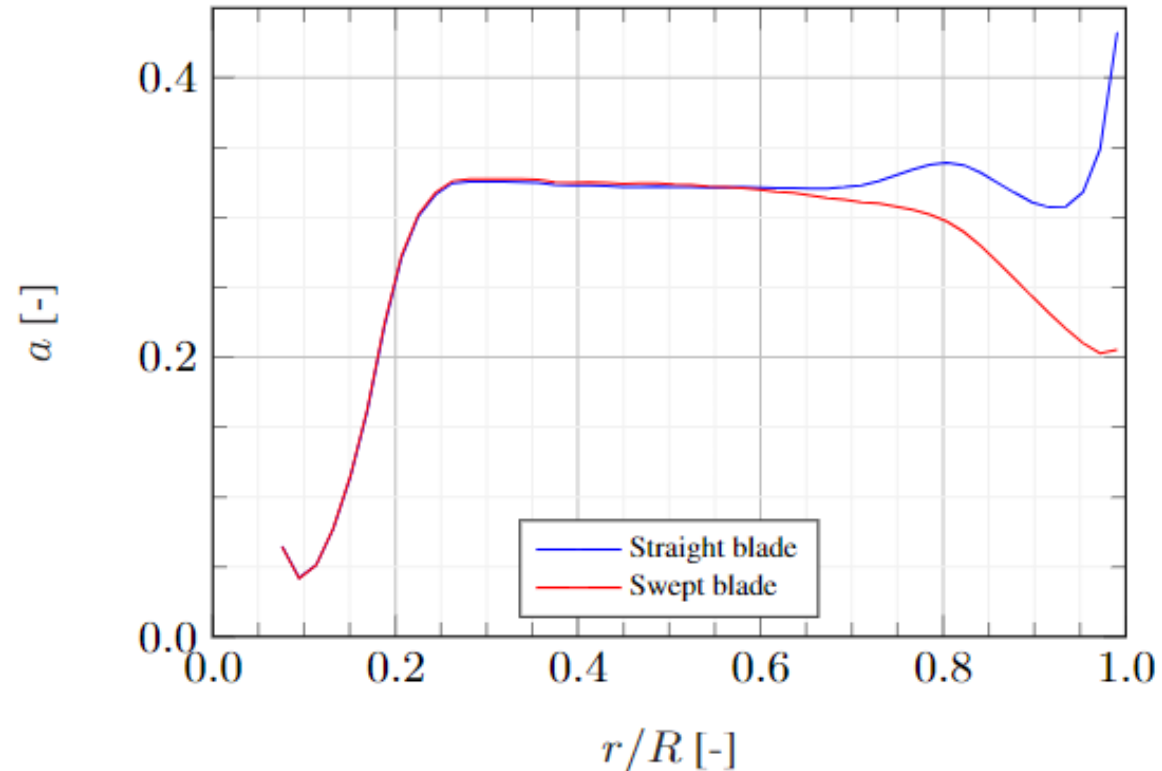
› Correct forces parallel to polar lift slope using BEM equations to correct for twist/pitch offset



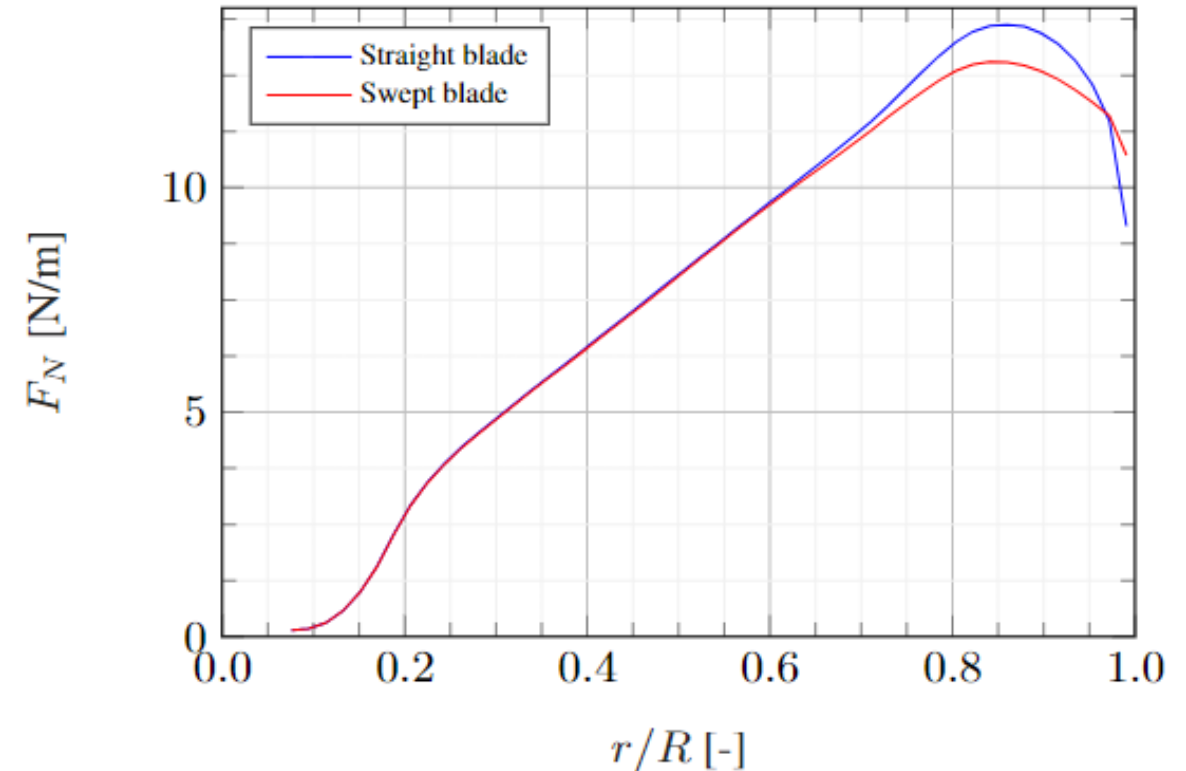
RESULTS

NUMERICAL SIMULATION

- › Axial induction drop-off towards the blade tip due to crossflow principle and displacement of the tip vortex



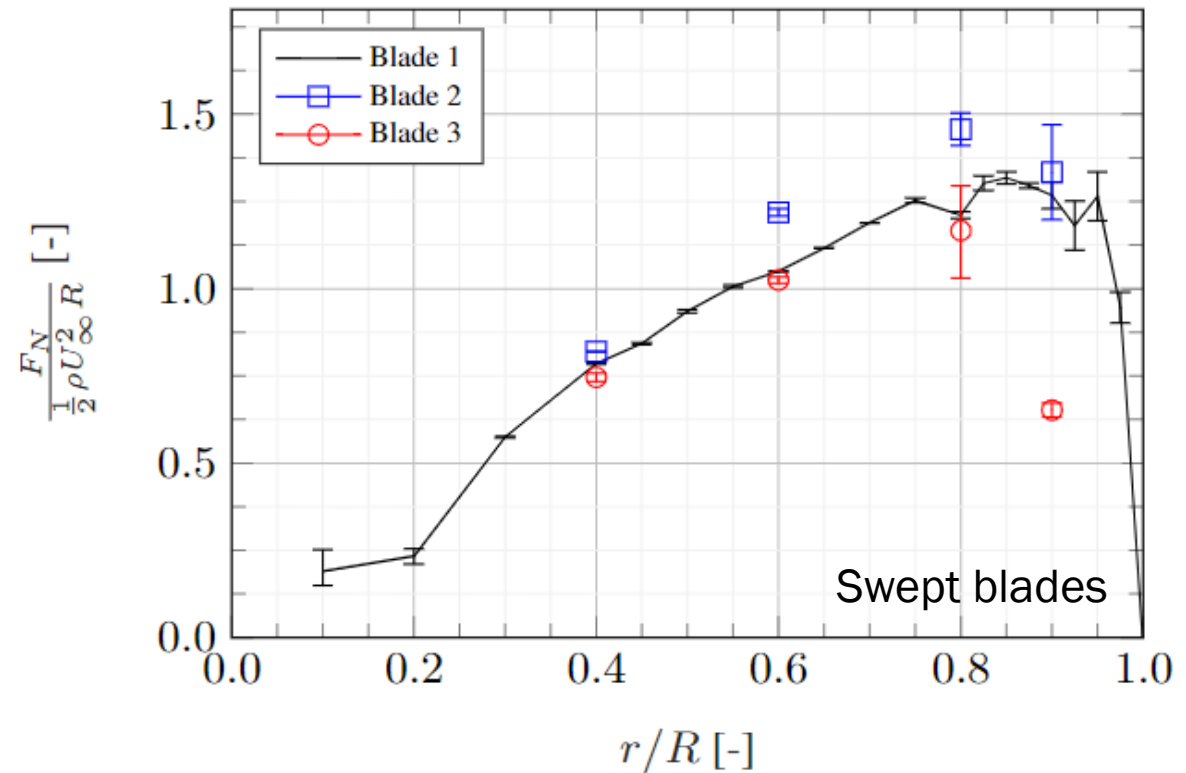
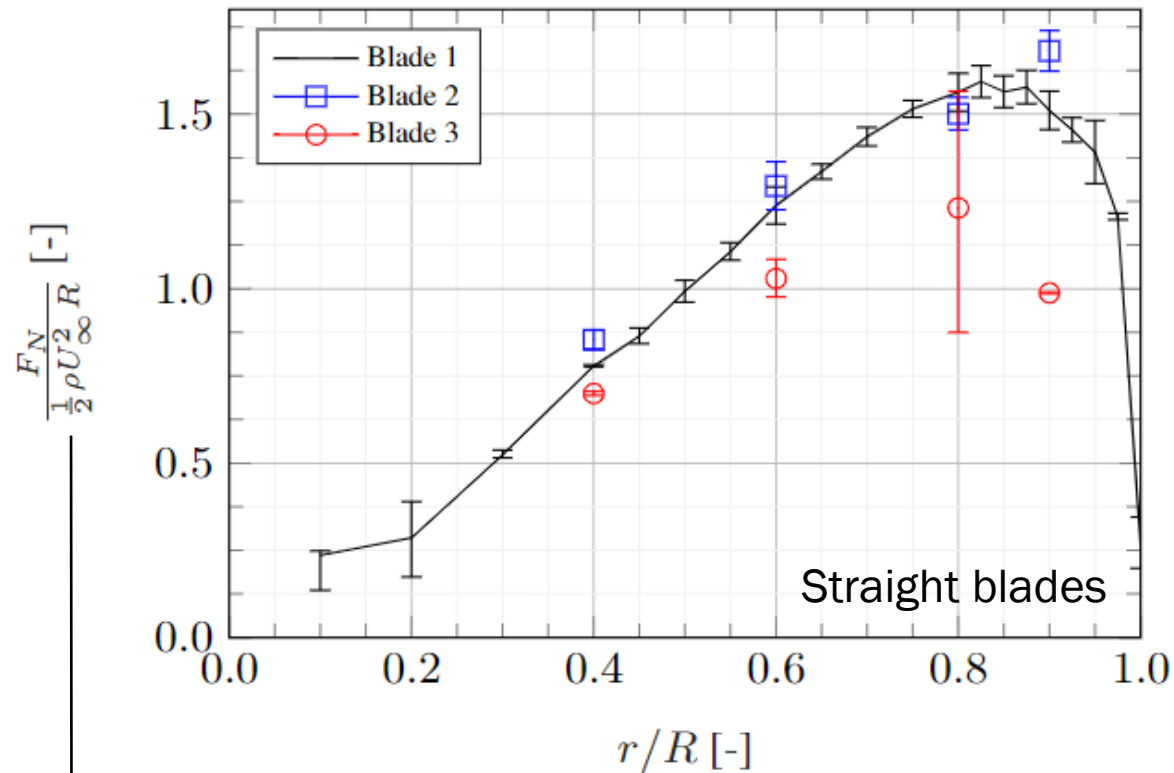
- › Consequently, also an axial force drop-off at the tip



RESULTS

EXPERIMENT – AXIAL FORCE, UNCORRECTED

› Uncorrected forces represent the expected trend

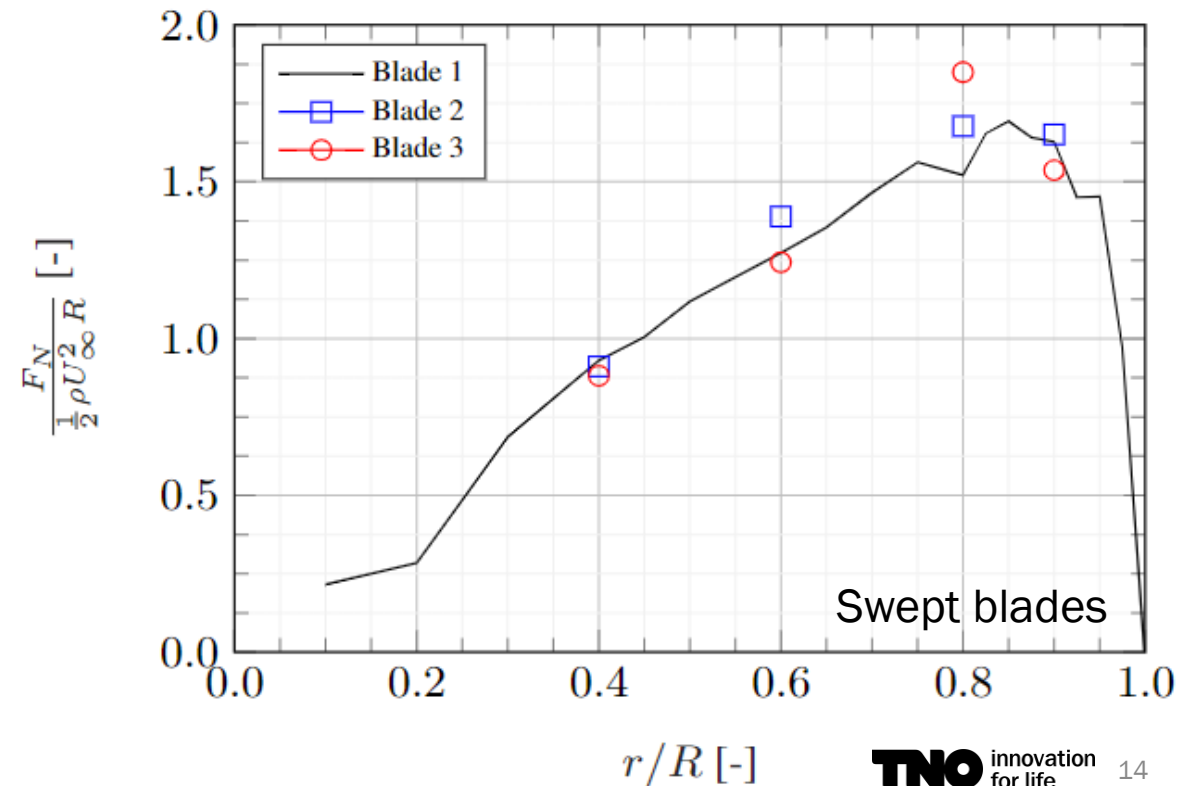
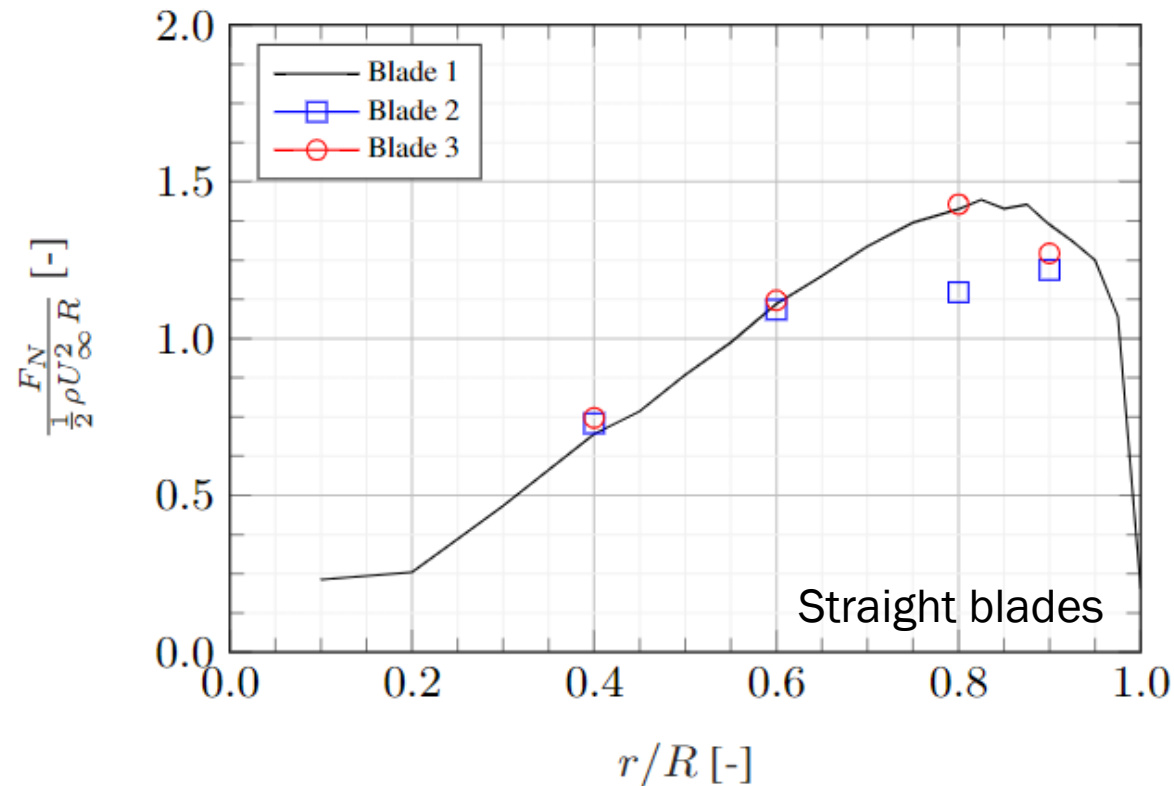


Non-dimensionalisation to account for slight changes in operating conditions

RESULTS

EXPERIMENT – AXIAL FORCE, CORRECTED

- › Corrected forces are **not** aligned with expectations
 - › Overall higher forces along the span, also at the geometrically identical inboard part of the blade
 - › Sweep-induced force drop-off not detectable



› CONCLUSIONS

› Achievements

- › Created an experimental database of a thrust-scaled IEA 15 MW model (flow fields, circulation, forces, induction values)
- › Created an experimental database of a rotating HAWT with swept blades

› Challenges

- › Manually manufactured blades exhibit varying stiffness properties
- › Manual pitch mechanism led to pitch offsets

› Future work

- › More accurately determine induction values
→ improving correction for pitch/twist offset
- › Use results for validation of numerical models



› **THANK YOU FOR
YOUR TIME**



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