

SEWGS technology is now ready for scale-up!





Available online at www.sciencedirect.com

SciVerse ScienceDirect

Procedia

Energy Procedia 37 (2013) 2265-2273

GHGT-11

SEWGS technology is now ready for scale-up!

Daniel Jansen^a, Edward van Selow^a, Paul Cobden^a, Giampaolo Manzolini^b, Ennio Macchi^b, Matteo Gazzani^b Richard Blom^c, Partow Pakdel Henriksen^c Rich Beavis^d and Andrew Wright^e

^a Energy Research Centre of the Netherlands (ECN), The Netherlands
^b Politecnico di Milano (PTM), Dipartimento di Energ, Italy
^c) SINTEF, Norway ^d) BP Alternative Energy, UK ^e) Air products PLC, UK

Abstract

In the FP7 project CAESAR, Air Products, BP, ECN, SINTEF and Politecnico di Milano worked together in the further development of the SEWGS process with the objective to reduce the energy penalty and the costs per ton of CO_2 avoided to less than ϵ 25 through optimization of sorbent materials, reactor and process design and smart integration of the SEWGS unit in a combined cycle power plant. The most promising applications for the SEWGS technology are IGCC power plants and in combined cycles power plants fuelled with blast furnace top gas.

Extensive sorbent development work resulted in a new sorbent called ALKASORB⁺ with a high capacity resulting in cost of CO₂ avoided for the IGCC application of \in 23. This is a reduction of almost 40% compared to the Selexol capture case. Since ALKASORB⁺ requires much less steam in the regeneration, the specific primary energy consumption is reduced to 44% below the specific energy consumption for the Selexol (2.08 versus 3.71 MJLHV/kg_{CO2}).

From a technical point of view SEWGS is ready to move to the next development level, which is a pilot plant installation with a capacity of 35 ton CO_2 per day. This is over 500 times larger than the current ECN's multi column SEWGS installation, but still 50 times smaller than an envisaged commercial scale installation. The pilot plant will prove the technology under field conditions and at a sufficiently large scale to enable further up-scaling, delivering both the basic design and investment costs of a full scale SEWGS demonstration plant.

© 2013 The Authors. Published by Elsevier Ltd. Selection and/or peer-review under responsibility of GHGT

Keywords: sorption-enhanced reaction; CO2 capture; IGCC; high temperature sorbent; costs and pilot plant

1. The concept of Sorption-Enhanced Water-Gas-Shift

The Sorption Enhanced Water Gas Shift (SEWGS) process is a novel pre-combustion decarbonisation technology that has the potential to reduce CO_2 capture costs versus conventional removal processes such as amine scrubbing. The process combines CO_2 adsorption with the water-gas-shift (WGS) reaction $CO + H_2O \leftarrow O_2 + H_2$. The process is executed with multiple vessels filled with catalytically active CO_2

adsorbent. When syngas (containing CO, H_2 , CO₂, H_2O , and inerts) is fed at high pressure and temperature (30 bar, 400 °C), CO₂ is removed by the sorbent. Hence, the WGS equilibrium is shifted to the right-hand-side, thereby completely converting the CO and maximizing the production of H_2 . This effectively removes CO and CO₂ from the feed gas, producing a high pressure, hydrogen rich product stream. Eventually though, the capacity of the adsorbent is saturated and CO₂ begins to appear in the product stream (breakthrough).



Figure1: Example of SEWGS cycle

At a predetermined level of CO_2 breakthrough, the bed is taken off-line and regenerated. Specific process steps are conducted for regeneration (based on pressure swing), and this produces a low-pressure by-product stream rich in CO_2 . By using multiple reactors/beds (6 to 9) and properly staggering the process cycle, the inherently dynamic process can mimic a continuous one, with essentially constant feed and product/by-product streams. The SEWGS process is particularly attractive for pre-combustion decarbonisation applications in IGCC and blast furnace gas. Here the desire is to convert as much CO in the fuel gas to H_2 as possible and then separate the CO_2 from the H_2 . The H_2 can then be fed to a gas turbine to generate power, while the CO_2 is sequestered.

Conventional approaches to this require multiple cooling steps. The first is to cool the hot gas from the high temperature WGS reactor to around 200°C to carry out a second low temperature WGS reaction to achieve the required conversion of CO. Further cooling is then necessary to enable the capture of CO_2 by absorption with a physical solvent. A more elegant and straightforward approach is offered by incorporating the SEWGS process. Partially shifted fuel gas from the high temperature WGS reactor is fed to a SEWGS unit, and a hot, high pressure, hydrogen rich product stream is directly produced. This H₂-rich product can be fed directly to a gas turbine at around 400 °C. This removes the inefficiency of cooling/heating of the H₂ that is an inherent part of the conventional process. In addition, the SEWGS technology can yield a CO_2 by product stream at sufficient purity for storage.

2. Test rigs

In the further development of the SEWGS process both the Single Column (SC) unit and the Multi Column (MC) test rigs at ECN were used for the long term testing of the sorbents, for the SEWGS

process model validation and for the cycle optimization. Next to that the high throughput sorbent test equipment at SINTEF was used in the search for new sorbents.



Figure 2: Test equipment used: Single Column (left) and Multi Column unit (middle) at ECN and high throughput unit (right) at SINTEF

3. Improving the performance of promoted hydrotalcite (K-HTC) sorbent

The CO_2 sorbent used at the start of the CAESAR project i.e. promoted hydrotalcite (K-HTC) showed unexplainable behaviour in the CO_2 sorption cycle and in the regeneration of the sorbent with steam. This reference hydrotalcite sorbent (denoted as K-MG70) showed poor mechanical stability (see figure 3) and increased CO_2 slip during long term testing under realistic conditions. It turned out that this was caused by the MgCO₃ formation which is a slow process.

A new HTC sorbent with a lower Mg content (K-Mg30) was selected for long term testing in the single column unit. During lab scale testing this K-Mg30 (called ALKASORB) sorbent showed good capacity so this sorbent was selected for long term testing in the single column unit. Although, the ALKASORB sorbent showed good overall performances, the techno-economic assessments showed that sorbent cyclic capacity must be increased with at least 50% (compared to the capacity of ALKASORB) in order to make the SEWGS process substantially cheaper than the more conventional capture technologies. In the fourth and final year, sorbent development resulted in a major breakthrough with respect to sorbent capacity. This ALKASORB⁺ sorbent has a 90% higher CO₂ capacity compared to ALKSORB and also uses less steam for the regeneration.



Figure 3: Sorbent unloaded from the reactor: (left) fractured K-MG70 HTC sorbent after more than 1200 cycles; (middle) mechanically stable ALKOSORB sorbent after more than 2000 cycles and (right) AlKASORB sorbent after three years testing in the SC unit.

The effect of contaminates in the syngas on the CO_2 adsorption capacity of the ALKASORB sorbent has also been investigated. The test with H₂S containing syngas showed clearly that ALKSORB also captures H₂S along with the CO_2 without significant loss of capacity. In separate tests, full COS hydrolysis and adsorption as H_2S followed by a simultaneous breakthrough of H_2S and CO_2 has been observed. Methane slips through completely whereas NH_3 is partially captured and HCH partially converted to NH_3 and partially captured. The test result clearly showed that ALKSAORB is a robust sorbent and capable of simultaneous decarbonisation and desulphurization of sour syngas originating from the gasification of coal. Accordingly, it produces a hot pressurised H_2 -rich product stream with low contents of CO_2 . COS and H_2S and next to a CO_2 rich stream with H_2S .

4. High throughput testing in search for new sorbents

In total 432 new sorbent formulations have been prepared, partly characterized and more than 300 sorbents have been evaluated under realistic conditions in a three cycle adsorption-desorption test (see figure 4). For the evaluation, a comparison with the reference HTC sorbents has been made, and four sorbent leads were selected for up-scaling and testing for sorption performance and particle stability under SEWGS conditions. However, none of these four sorbents performed sufficient to scale up the sorbent for testing in the single-column and multi-column rigs.



Figure 4: Example of a high throughput test result. CO₂ adsorption capacity of new sorbents is benchmarked against the reference HTC ALKASORB sorbent.

5. Catalyst testing

In conventional shift applications, the catalyst operates under reducing conditions. For application in a SEWGS process the catalyst should be able to withstand the oxidising conditions during the cycle, such as during the sorbent regeneration by steam. It should also remain active at the SEWGS operating conditions where only a limited amount of steam in the feed is present. Commercially available catalysts on supports have been benchmarked at different temperatures and in the presence of actual CO_2 sorbents. However, during breakthrough experiments with promoted hydrotalcite under realistic conditions it was observed that even in the absence of a catalyst the carbon monoxide in the feed gas was completely shifted to carbon dioxide (see figure 5). A stability test showed the stability of the sorbent working capacity as well as shift activity during 5000 cycles, at a minimal steam to carbon ratio (2 mole/mole). Hence, it was demonstrated that the SEWGS process does not require a shift catalyst, which brings substantial economic and technical benefits for this technology.



Figure 5: ALKASORB breakthrough tests without catalyst showing sufficient WGS activity before CO2 breakthrough!

6. Process modeling

Using the experience with conventional PSA units along with the fundamentals learnt from the singlecolumn tests at high temperature, a dedicated SEWGS process has been developed. Experimental data from the multi-column rig was used to validate the model and enabled corrections to be made for those steps in the cycle that were not present in the single-column tests. The model was used for cycle optimisation and to study different plant lay outs i.e. vessel size, vessel number, regeneration medium, pressure etc. and provided insight in ways to improve the SEWGS process both technically and economically. Table 1 and figure 6 provide excerpts of the modelling results for the SEWGS application in an IGCC power plant.



Figure 6: Example of SEWGS process modelling results for application in an IGCC power plant; Carbon capture rate (left) and CO₂ purity (right) as function of purge and rinse flow.

The carbon capture rate can be improved by increasing the amount of purge steam used as this desorbs more CO_2 from the sorbent, allowing more CO_2 to be adsorbed during the feed step for the same cycle time. The modelling work also shows that increasing the rinse gas flow rate results in an improved CO_2 product purity as it pushes more of the H₂-rich gas out of the beds after the feed step. The overall result of the modelling work is that the flows of rinse and purge gas must be balanced against each other to achieve the required carbon capture rate and CO_2 purity. The effect the carbon capturer ratio on the net efficiency for an IGCC power plant is illustrated in table 1.

SEWGS in IGCC application	SEWGS CCR 98%	SEWGS CCR 95%	SEWGS CCR 90%
Net Electric Efficiency _{LHV} , [%]	37.6	38.5	39.3
Emissions, [g _{CO2} /kWh _{el}]	22	48	88
CO ₂ avoided, [%]	96.93	93.4	87.8

Table 1: IGCC efficiency, CO2 emissions and CO2 avoidance rate for different capture ratios

7. SEWGS applications

The ideal application for advantaged integration of the SEWGS process would be combination with a process which can fully exploit the following SEWGS characteristics:

- High temperature hydrogen (typically 400°C)
- High pressure hydrogen (typically 30bar)
- Medium purity hydrogen (typically 90-95 mol%)
- High temperature CO_2 (typically 400°C)
- CO₂ at ambient pressure
- High CO conversion

Power application

In a combined cycle power production unit with CO_2 capture by pre-combustion, the process will be enhanced by the production of high temperature hydrogen, making the SEWGS process potentially advantaged for this application. As the requirement for CO_2 removal (and hence hydrogen purity) is not very stringent, processes such as SEWGS which don't produce high separation factors, would not be penalised by the requirements for further polishing steps. So SEWGS fits with power production with CO_2 capture.

Non Power applications

Non power applications have been assessed on the basis of the typical characteristics of the SEWGS technology mentioned above. The applications that are being assessed are:

- Distributed Refinery Hydrogen
- Refinery Process Hydrogen
- Refinery Fuel Gas
- Ammonia production
- Coal to liquid chemicals & liquid fuel

The assessment made clear that these non power application cannot fully exploit the SEWGS characteristics and therefore these non power applications are less obvious with likely lower economic benefits.

8. Techno economic assessments

The techno economic assessment for the SEWGS application in an IGCC power plant bas been performed on basis of the results of the extensive ALKASORB testing in both the single column and multi column test rig and the SEWGS cycle optimisation and cost estimates. The results are summarised in table 2. In the final year of the CAESAR project, work to improve the capacity of AKASORB sorbent continued and resulted in a better sorbent (ALKASORB⁺) with a substantial higher capacity and consequently improved performance data (see also table 2).

Calculated cost of electricity and cost of CO_2 avoided for SEWGS in IGCC and reference IGCC cases are summarized in table 2. The COE for the reference case IGCC is about 66 ϵ /MW_h. More than 50% of the COE depends on the investment costs, while fuel costs account for about 35%. This result is typical for coal based plants; while natural gas based plants have an opposite trend. COE for the CO₂ capture cases increases 35% because of the higher investment cost as well as higher fuel costs. The resulting cost of CO₂ avoided is 36.7 ϵ /t_{CO2} which is in the range of similar studies proposed in literature supporting the reliability of this analysis.

The application of SEWGS ALKASORB in an IGCC allows reducing the cost of electricity to about 86 €/MWh i.e. 3.5% less than in the SELEXOL case. The avoidance rate of SEWGS ALKASORB is however, over 7% points higher. SEWGS reduces investment and also the fuel costs due to the co-capture of sulfur and consequent equipment costs savings, and the higher efficiency. Only consumables, which mainly depend on sorbent replacement, are higher. With the new ALKASORB⁺ sorbent the COE is reduced to 82.3 €/MWh. Accordingly, the cost per ton of CO₂ avoided is reduced to approx. 23 € which is a reduction of more than 35% compared to the Selexol capture case. Due to the fact that ALKASORB⁺ requires much less steam, the specific energy consumption is substantially reduced to 44% below the specific energy consumption for the Selexol (2.06 versus 3.67 MJLHV/kg_{CO2}).

	IGCC	Selexol	SEWGS ALKASORB	SEWGS ALKASORB+
SEWGS CCR/CO2 purity	-	-	95/99	95/99
Net Power Output, [MW]	422.4	379,6	393.1	404.2
Thermal Power Input _{LHV} , [MW]	896.5	1053.5	1020.6	1017.0
Net Electric Efficiency (LHV base), [%]	47.12	36.03	38.5	39.75
CO ₂ avoided, [%]	-	86.5	92.8	93,7
SPECCA [MJ _{LHV} /kg _{CO2}]	-	3.71	2.51	2.08
Specific costs, €/kW	2093.0	2888.1	2867.0	2603,2
COE, [€/MWh]	66,3	89.55	86.52	82.27
Cost of CO ₂ avoided [€/t _{CO2}]	-	36.7	31.2	23.4

Table 2: Cost of Electricity and Cost of CO2 avoided for the two SEWGS cases and for the reference IGGC cases

9. Technology readiness level and pilot installation

The SEWGS technology was evaluated using NASA's technology readiness level methodology and classified on level 5-6. At the end of the CAESAR project (December 2011) SEWGS development was ready to move to the next development level, which is a pilot plant installation of which the capacity is on the order of 500 times larger than the current multi-column Process Development Unit, but still 50 times smaller than a commercial scale installation .

The primary objectives of a pilot plant are:

- Prove SEWGS performance on sufficient scale and under field conditions
- Confirm scale-up parameters and assurance of modelling results
- Prove the design is fit for purpose
- Optimise the cycle design

The main requirements of a pilot unit include availability of syngas, power, steam, nitrogen, cooling fluid, instrument air, process water, waste disposal of condensate, CO_2 and H_2 . Furthermore, an inventory of critical items for the SEWGS technology was made. These issues will be addressed in the pilot project. In the course of 2012 a suitable host site was identified, and a SEWGS pilot validation project proposal was made. The pilot project is scheduled for the period 2013 - 2016.

10. Vessel design and availability of high-temperature valves

For the mechanical design of the vessels, the frequent pressure swings are of critical importance for the fatigue analysis. Several design alternatives were proposed and assessed taking into account the applicable codes and standards, and the best design was selected. Cost estimations for this vessel were obtained. Specifications for the high-temperature valves were made, using the optimised configuration of vessels and valves established earlier in the project. The availability and prices of the valves were obtained from vendors. Various suitable valves were identified, and valve availability did not appear to be an issue, although delivery times could be substantial.



Figure 7: Impression of a 3D design for a commercial size SEWGS unit, capturing 1500 ton CO₂ per day

11. Conclusion

The pre combustion CO_2 capture technology SEWGS is particular suited for the de-carbonization and desulphurization of sour syngas originating from coal gasification. Most favourable SEWGS applications are therefore in IGCC power plants and in combined cycle power plants fuelled with blast furnace top gas.

The newly developed ALKASORB class sorbents are very robust i.e. have a good chemical and mechanical stability, are WGS catalytic active and have total steam to carbon ratio of less than 2 (mole/mole) for regeneration.

Application of the ALKASORB⁺ sorbent with the 90% higher CO₂ capacity compared to ALKSORB and the 60% lower steam use in the regeneration, results in a cost of CO₂ avoided for the IGCC application of \notin 23 and a primary specific energy consumption of 2.08 MJ_{LHV}/kg_{CO2}). Overall, the SEWGS

The SEWGS technology has progressed to a technology readiness level of 6 and is now ready for scale up and pilot testing at a capacity of 35 ton CO_2 with a real coal based syngas. The pilot plant will prove the long term stability of the ALKASORB sorbents and the reliability of key equipment, particularly high temperature valves, will confirm scale up parameters and assurance of modelling results.

Acknowledgements

The research leading to these results has received funding from the European Community's Seventh Framework Programme under grant agreement no. 213206.

References

[1] Andrew Wright, Vince White, Jeffrey Hufton, Edward van Selow, Peter Hinderink. Reduction in the cost of pre-combustion CO₂ capture through advancements in sorption-enhanced water-gas-shift. *Energy Procedia* 1 (2009) 707–714

[2] Van Selow ER, Cobden PD, Van den Brink RW, Wright A, White V, Hinderink P, Hufton JR. Pilot-scale development of the sorption enhanced water gas shift process. *In: Eide LI, editor. Carbon dioxide capture for storage in deep geologic formations, Berks*, CPL Press; 2009, p. 157-80.

[3] Van Selow ER, Cobden PD, Wright AD, Van den Brink RW, Jansen D. Improved sorbent for the sorption-enhanced watergas shift process. *Energy Procedia 2011*; 4: 1090-5.

[4] Walspurger S, Cobden PD, Safonova OV, Wu Y, Anthony EJ. High CO2 Storage Capacity in Alkali-Promoted Hydrotalcite-Based Material: In Situ Detection of Reversible Formation of Magnesium Carbonate. *Chem Eur J* 2010; 16 (42): 12694–700.

[5] Egil Bakken, Paul D. Cobden, Partow Pakdel Henriksen, Silje Fosse Håkonsen, Aud I. Spjelkavik, Marit Stange, Ruth Elisabeth Stensrød, Ørnul Vistad, Richard Bloma. Development of CO₂ sorbents for the SEWGS process using high throughput techniques. *Energy Procedia* 4 (2011) 1104–1109

[6] Wright AD, White V, Huftonb JR. Quinn R, Cobden PD, Van Selow ER, CAESAR: Development of a SEWGS model for IGCC. *Energy Procedia* 4 (2011) 1147–1154

[7] Van Dijk HAJ, Walspurger S, Cobden PC, Van den Brink RW, Testing of hydrotalcite based sorbents for CO₂ and H₂S capture for use in sorption enhanced water gas shift. *Int J Greenhouse Gas Control* 2010; 5 (3): 505-11

[8] Van Selow ER, Cobden PD, Verbraeken PA, Hufton JR, Van den Brink RW. Carbon capture by sorption-enhanced water gas shift reaction process using hydrotalcite-based material. *Ind Eng Chem Res* 2009; 48 (9): 4184-93.

[9] Gazzani M et al. CO2 capture in integrated gasification combined cycle with SEWGS – Part A: Thermodynamic performances. *Fuel* (2012), http://dx.doi.org/10.1016/j.fuel.2012.07.048.

[10] Manzolini G et al. CO2 capture in Integrated Gasification Combined Cycle with SEWGS – Part B: Economic assessment. *Fuel* (2012), http://dx.doi.org/10.1016/j.fuel.2012.07.043



ECN

Westerduinweg 3 1755 LE Petten The Netherlands P.O. Box 1 1755 LG Petten The Netherlands

T +31 88 515 4949 F +31 88 515 8338 info@ ecn.nl www.ecn.nl