23% Efficiency Metal Wrap Through Silicon Heterojunction Solar Cells

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Abstract — MWT-SHJ cells and modules combine the positive benefits of both underlying technologies: namely high V_{oc}, higher J_{sc} and higher FF. Especially the FF is maintained before and after encapsulation thanks to the rear interconnection which strongly reduces cell to module FF losses. We obtained two record efficiencies for these devices with two different front metallizations: 22.6% using low temperature Ag paste and 23.1% using copper plating. V_{oc} values above 730 mV have been achieved also in the new 6x6 vias metallization, demonstrating that the architecture maintains the exceptional passivation typical of heterojunction devices. The MWT cell and module structure offers even greater advantages on heterojunction solar cells: i) front side Ag consumption reduction up to a factor two; ii) concurrent low temperature cell interconnection and encapsulation. Our record MWT-SHJ solar cells and modules are manufactured using industrially proven tools and 6 inch commercial n-type Cz Si wafers. The metallization choice gives ample room to manufacturers for optimization based on internal cost structure, material costs and business strategy, MWT-SHJ behavior at reverse bias voltage and low illumination intensity is comparable to conventional HJ devices.

I. INTRODUCTION

High efficiencies and low materials consumption are the main drivers towards low-cost (\$/Wp) silicon PV modules.

Several solar cell technologies have demonstrated the ability to reach 22% cell efficiency. In addition, new back contact module technologies are now available to overcome losses caused by the interconnection and due to the limited width of the tabs.

In this contribution we show the most recent development in the successful combination of Metal Wrap Through (MWT) architecture with Silicon Heterojunction (SHJ) solar cells.

The vast majority of the market implements module technologies based on interconnection of solar cells in strings by tabs soldered from the front of one cell to the rear of the adjacent one. To limit shading losses caused by these tabs, such interconnection leads to additional resistive losses in a string of cells thereby reducing the module performance. MWT technology provides a relatively small step from conventional cell technologies and has already demonstrated to increase the module power by 3%, and up to at least 5% is anticipated [1]. This is possible thanks to an integrated cell and module design in which conductive interconnection foil is used to eliminate cell-to-module power loss compared to conventional tabbing technology. Part of this gain is thanks to the reduced metal coverage on the front side, giving the solar cell performance a potential efficiency increase up to about 2.5% relative. Furthermore, thanks to the unit cell concept (the front contact of each unit cell connected to a rear contact by a through-cell via), MWT cell structure decouples the wafer size from metallization requirements allowing for better cell-to-module power ratio.

Front and rear contacts heterojunction solar cells have demonstrated more than 24% cell efficiency (25.6% on interdigitated back contact [3]) achieving excellent surface passivation with Voc exceeding 730 mV [2]. Furthermore SHJ has a lower temperature coefficient, resulting in higher module energy yield under real operating conditions.

Nevertheless the low temperature Ag paste required for contact formation in SHJ devices is still today a challenge as it suffers from high cost and low conductivity resulting in high Ag consumption. Solutions such as multi-wire interconnection and multi-busbars have been introduced to tackle this conductivity issue [4,5].

MWT-SHJ architecture provides an elegant solution to high cost and reduced conductivity of low temperature silver pastes while maintaining the above mentioned advantages of SHJ.

Moreover, the low-temperature process required by heterojunction is perfectly met by the soldering-free MWT module technology which uses conductive adhesive and single step curing for interconnection and encapsulation.

MWT and SHJ cell technologies are also compatible with next generation thinner wafers resulting in a win-win situation both on cell and module level.

MWT-SHJ devices combine all the advantages of the individual concepts in a device with high open circuit voltage, high short circuit current and high module power thanks to reduced power loss.

In this paper, we show the most recent results of this MWT-SHJ solar cell architecture which resulted in a record efficiency of 23% total area using commercial n-type Cz 6 inch wafers.

II. PURPOSE OF THE WORK AND APPROACH

In this contribution we describe recent development of metal wrap through (MWT) silicon heterojunction (SHJ) solar cells and modules. We used a rear emitter cell structure to reduce recombination and shunt at the vias as previously reported [6]. Our approach is both theoretical and experimental. We used a 2D model to predict the experimental results and chose the best configuration and geometry of the MWT unit cells. The model has been then validated by

fabricating real working devices and characterization (IV-curve and EL).

In addition here we demonstrate this approach with both low temperature Ag paste screen printing and Cu plating.

III. SCIENTIFIC INNOVATION AND RELEVANCE

To our knowledge, the solar cell performances obtained are record efficiency for both MWT-SHJ and MWT devices. The use of conventional low temperature Ag paste and low temperature interconnection methods (i.e. conductive tape, multi wire etc.) provide a costly solution that hinder the entrance in mass production of Si heterojunction technology. MWT-SHJ addresses both issues. The MWT structure allows the reduction of the current to be transported thanks to the reduction of the unit cell size at virtually no-cost and without the complicated hassle of upscaling to multi-busbar or multiwire (high T) or smart-wire (low T) technologies. This allows a reduction of front Ag CoO up to a factor two accounting both the front side metallization and interconnection. We expect a similar gain from the rear metallization. On module level, the cells are interconnected through the conductive rear side foil by means of conductive adhesives. During lamination, interconnection takes place at low temperature concurrently to encapsulation.

IV. CELL STRUCTURE

MWT solar cells have the same architecture of a conventional solar cell with the addition that the front metal contact is wrapped through the wafer through metallized via holes, providing both emitter and base contacts on the rear side (Fig. 1) [6]. As the cell interconnection does not require tabbing and MWT unit cell can be reduced independently from wafer size, the busbar are significantly slimmed down enhancing the light harvesting in comparison to conventional H-pattern cells.



Figure 1. Structure of a rear emitter MWT-SHJ solar cell. The diagram is not in scale. The collecting layer represents both the TCO and Ag rear contact.

V. EXPERIMENT AND RESULTS

6" industrial n-type Cz monocrystalline full-square silicon wafers about 180 µm thick were used as substrate for MWT-SHJ solar cell fabrication. Conventional heterojunction processing sequences were used for the fabrication of the solar cells: texturization and cleaning, a-Si:H deposition by PECVD and TCO deposition. The MWT-SHJ solar cell process is the same as the SHJ process with adding a few extra steps typical for MWT cell technology [1]: vias drilling, via filling and isolation of the two metal contacts at the rear. In this experiment, the vias drilling is done before the surface preparation for the a-Si:H depositions, therefore the damage removal is done without adding any extra chemical step. In the MWT-SHJ process used, an isolation of the metal plug from the underlying Si or a-Si:H layer is not necessary. The via filling is done within the same printing step of the rear side pad.

Two types of metallization have been used: i) low temperature silver paste by screen printing and ii) Copper plating of the front metallization. The copper plating has been entirely developed by CIC. A description of this process is described in a sister publication [7].

The rear side of both devices is identical and it can be carried out in two different ways: i) by screen printing and ii) by PVD (Ag blanket).

Structure	Front	Jsc	Voc	FF	Eta
	metal	(mA/cm²)	(mV)	(%)	(%)
H-pattern	Ag 3BB	38.9	722	77.3	21.7
MWT 4x4	Ag	39.1	726	76.6	21.7
MWT 6x6	Ag	39.2	723	77.6	22.0
MWT 6x6	Ag	39.3	719	80.0	22.6

Table I. IV-results of the MWT-SHJ solar cells. Cell area 243 cm². Total area efficiency

In table I and Fig. 2, all the cells are measured at ECN according to the ASTM-E948 norm using a Wacom class AAA solar simulator and spectral mismatch correction. Solar cell efficiency is total area.

The first three devices in Table I are manufactured in the same batch to compare the different configuration (front and rear contacts, MWT with 4x4 vias and MWT with 6x6 vias). Only the busbar width and number have been changed from configuration to configuration as in MWT the current transport is carried out in the rear side. The number and width of fingers have been kept constant (same finger metal coverage). This allowed making a direct comparison among the different configuration. The total front metal shading for the three devices is 5.6%, 3.7% and 3.4% for the 3BB, MWT

4x4 and MWT 6x6, respectively. The last development carried out with LT-Ag metallization (4th cell in Tab I) consists in reducing the rear dead emitter area by about 30% as suggested in [6]. The dead emitter area reduction is estimated to improve the efficiency by 0.2% (mostly due to FF). At the same time the a-Si deposition was improved resulting in an efficiency gain of 0.6%.

We estimated that with 6x6 configuration and optimizing the finger width and spacing, the CoO of the front LT-Ag can be reduced by 30% [6]. This can be further reduced up to 50% increasing the number of vias [6].

In order to show the potentiality of the MWT-SHJ architecture, Cu plating has been applied to this device structure. The front metallization pattern has been improved using a radial pattern. This has allowed to increase the J_{sc} and V_{oc} , while keeping similar FF. The IV-curve is shown in Figure 2.



Figure 2. IV curve best cell with front cupper plating measured at ECN according to the ASTM-E948 norm using a Wacom class AAA solar simulator and spectral mismatch correction. Total area efficiency.

In our MWT-SHJ, we demonstrate J_{sc} superior of conventional H-pattern SHJ thanks to the reduced metal front coverage as result of the carrier transport transferred to the rear side. In addition the FF increases on cell level since the current transport is not limited by the busbar width and by their number. The effect on the FF is more evident on module level. In fact the measurement setups for H-pattern and MWT-SHJ solar cells are different. For the H-pattern multi-probes are usually used for the front contact of the cells. These increase the conductivity of the busbar independently of their width and thickness which results in higher FF (see table I Hpattern ref versus 4x4). This is not the case in real conditions (interconnection within the module) since the tabs used for the interconnection have a more limited conductivity than the multi-probes. MWT-SHJ measurements chucks do not use multi-probes as the current is transported to the rear side only thanks to the front metallization. The result is that the measurement is carried out in real module conditions. Therefore a real comparison of the performance of MWT-SHJ and conventional front and rear contact architectures should be carried out on module level where absence of cell to module loss will be evident.

A. Reverse characteristics

MWT-SHJ I_{rev} current are less than 0.5 A at -10 V for both 4x4 and 6x6 configuration (see Fig. 3) similarly to convention H-pattern SHJ.



Figure 3. Reverse characteristic of MWT-SHJ solar cells with Ag screen printing.

B. Sensitivity to illumination

In order to study the behavior of the MWT-SHJ solar cells in condition of low illumination we measured their power at different illumination levels. We measured both heterojunction H-pattern and MWT-SHJ solar cells as shown in Figure 4.



Figure 4. Efficiency versus illumination.

No particular difference in the illumination response for MWT-SHJ solar cells with respect to conventional H-pattern silicon heterojunction solar cells. This indicates that shunt resistance impact, if any, in MWT-SHJ is comparable to that of conventional front and rear contacts H-pattern heterojunction devices.

IV. CONCLUSIONS

We demonstrated MWT-SHJ solar cells with record efficiencies of 23.1% and 22.6% fabricated with copper plating and low temperature Ag paste, respectively. In the current configuration with LT-Ag paste and 6x6 vias we estimated a 30% CoO reduction on Ag consumption with options to further reduce it to 50% with respect to 4x4 vias no-extra manufacturing complexity. with The two metallization concepts are not yet fully optimized and there is further room for efficiency gain. Solar cell behavior is comparable to conventional HJ at reverse bias voltage and low illumination intensity.

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