

Immersed Actuator Methods

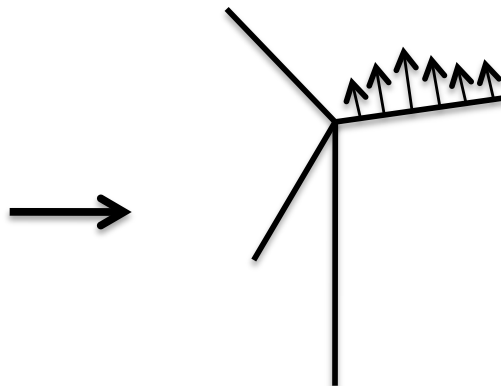
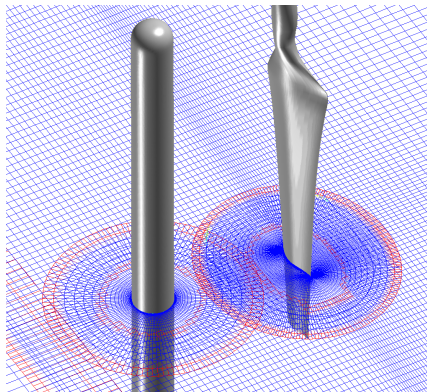
B. Sanderse, B. Koren

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11-10-2012

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Introduction

- Actuator methods for wind-turbine wake aerodynamics:
 - Circumvent meshing entire rotor blade
 - Circumvent resolving blade boundary layer
 - Actuator disk, line, surface, ...



Existing methods

- Actuators as volumetric body forces (Sørensen et al.)
 - Cartesian mesh
 - Discrete Dirac functions, regularization parameter
 - Time steps limited by movement of lines
- Actuators as singular surface forces (Masson et al.)
 - Surfaces carrying discontinuities in pressure and velocity
 - Body-fitted meshes
 - Based on inviscid aerodynamic theory
- Actuator shape model (Rethore)
 - Forcing based on intersectional polygon between actuator and mesh

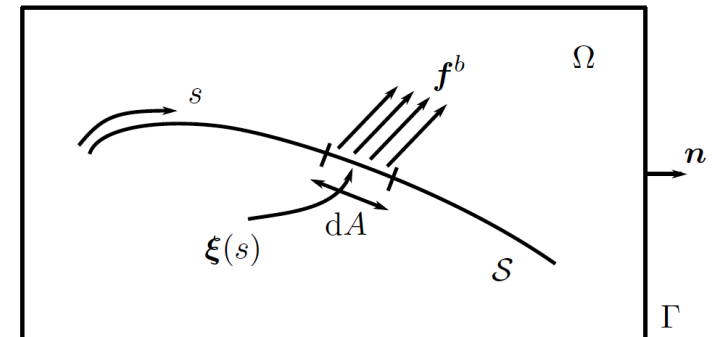
Forces in the Navier-Stokes equations

- **Surface forces in integral form**

$$\int_{\Omega} \frac{\partial \mathbf{u}}{\partial t} d\Omega + \int_{\Gamma} \mathbf{u} \mathbf{u} \cdot \mathbf{n} d\Gamma = \int_{\Gamma} -p \mathbf{n} d\Gamma + \int_{\Gamma} \nu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) \cdot \mathbf{n} d\Gamma + \mathbf{F}$$

$$\mathbf{F} = \int_{\mathcal{S}} \mathbf{f}^b(\boldsymbol{\xi}(s)) dA$$

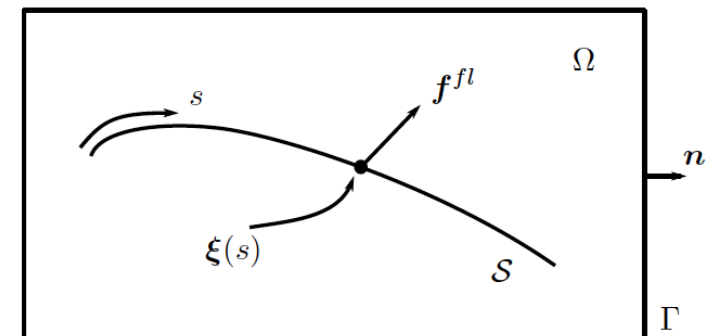
– Examples: pressure forces, shear forces (C_p, C_f)



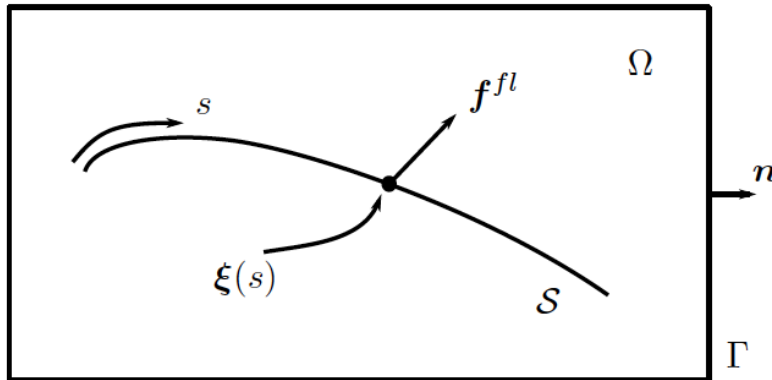
- **Volumetric forces in differential form**

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \nu \nabla^2 \mathbf{u} + \mathbf{f}^{fl}(\mathbf{x})$$

$$\mathbf{f}^{fl}(\mathbf{x}) = \int_{\mathcal{S}} \mathbf{f}^b(\boldsymbol{\xi}(s)) \delta(\boldsymbol{\xi}(s) - \mathbf{x}) dA$$

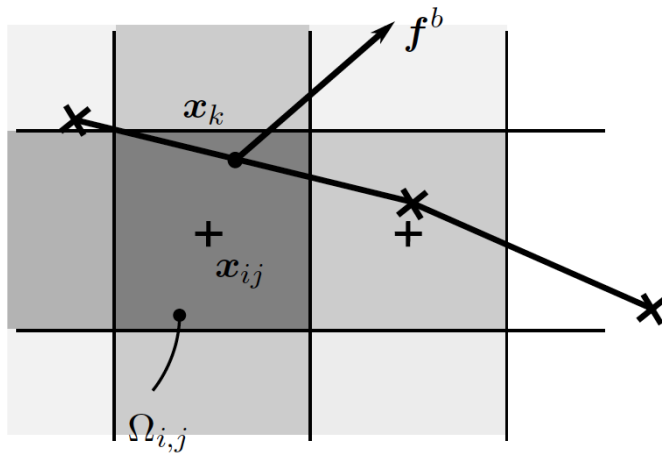


Standard approach



continuous

$$f^{fl}(x) = \int_S f^b(\xi(s)) \delta(\xi(s) - x) dA$$

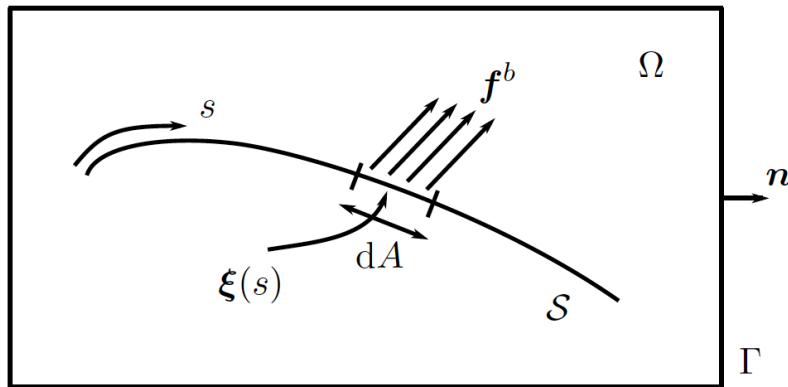


discrete

$$f_{ij} = \sum_k f_k d(x_k - x_{ij})$$

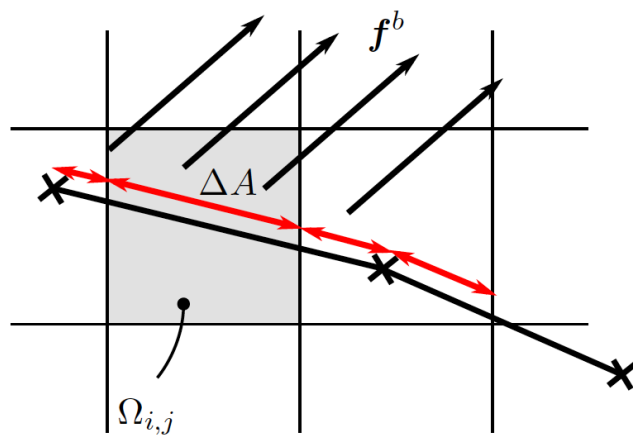
discrete Dirac function

New approach



continuous

$$F = \int_S f^b(\xi(s)) dA$$



discrete

$$f_{ij} = f^b \Delta A$$

No discrete Dirac function required, but ...

Discontinuities

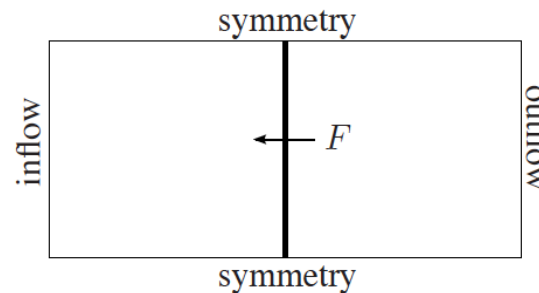
- Surface forces induce discontinuities

velocity is continuous $[u] = 0$ $\left[\mu \frac{\partial u}{\partial n} \right] = -f_{\tau}^b \tau$

pressure jumps $[p] = f_n^b$ $\left[\frac{\partial p}{\partial n} \right] = \frac{\partial f_{\tau}^b}{\partial s}$

- Example: 1D actuator disk – pressure jumps due to normal force

$$\Delta p = -\frac{1}{2} C_T$$



Handling discontinuities

- Discrete Dirac functions:
 - Easy implementation
 - Diffuse interfaces
 - Choice of Dirac function and regularization parameter
 - First order accurate in general
- Immersed interface methods (IIM)¹:
 - **Take jump conditions as corrections into discretization scheme**
 - Second order (or higher) accurate
- **Immersed actuator methods (IAM):**
 - IIM in finite volume framework
 - Application to actuators

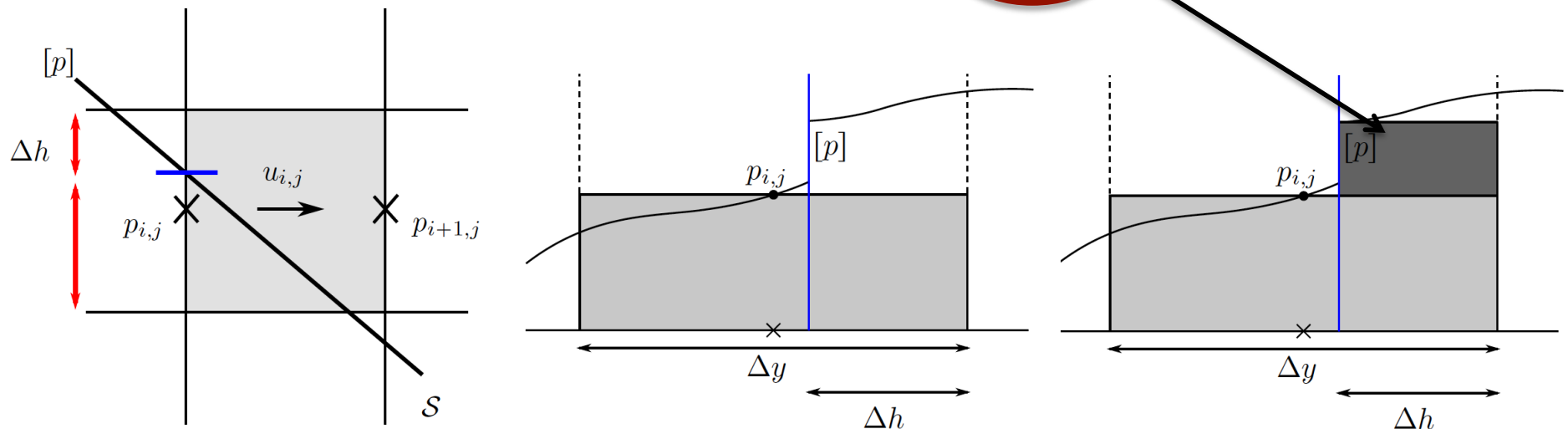
1: Z. Li and K. Ito, The Immersed Interface Method. Numerical Solutions of PDEs Involving Interfaces and Irregular Domains, SIAM 2006.

IAM applied to Navier-Stokes

- Apply the IAM to the pressure gradient term:

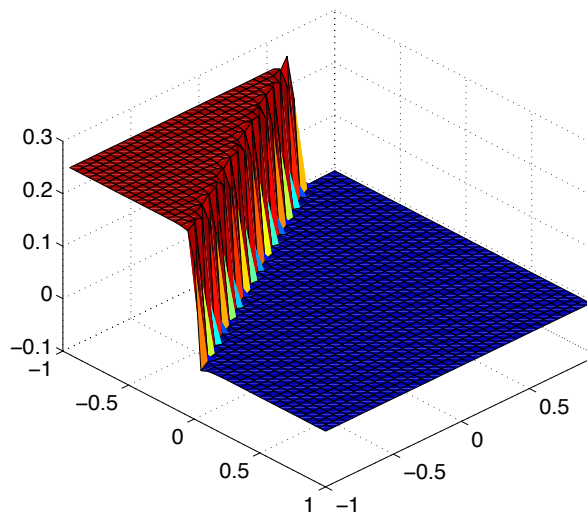
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- Jump correction: $\int p n_x dy = p_{i,j} \Delta y + [p] \Delta h$

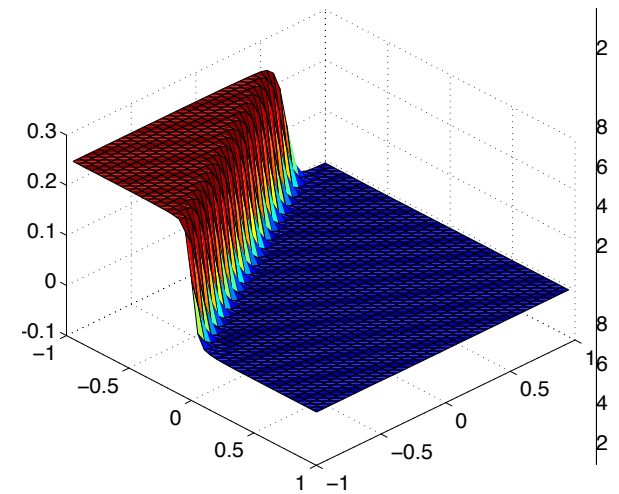
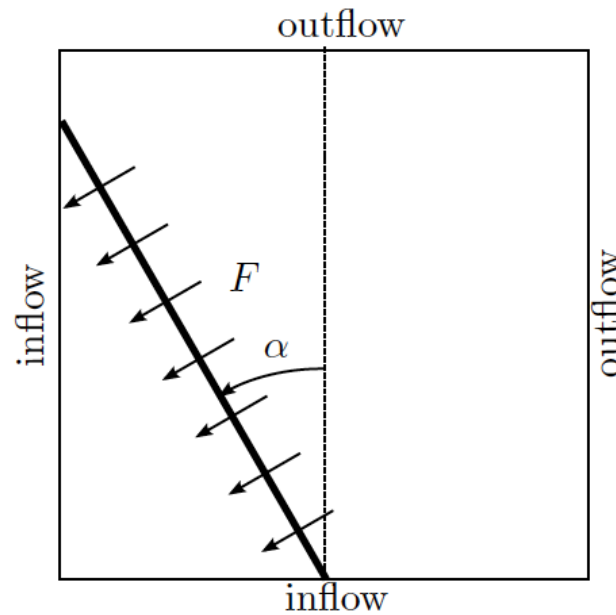


Quasi-1D actuator disk

- Actuator disk under angle in uniform flow
- IAM gives exact solution

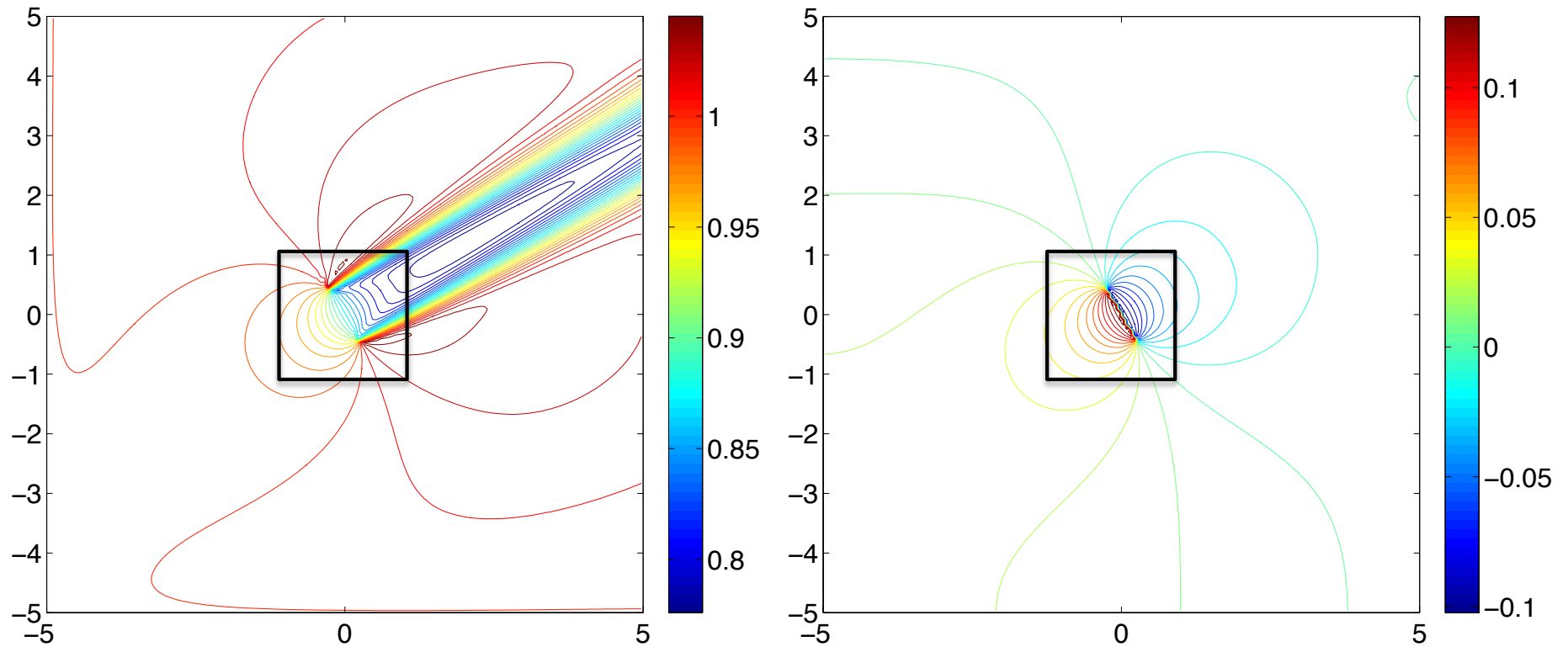


no corrections

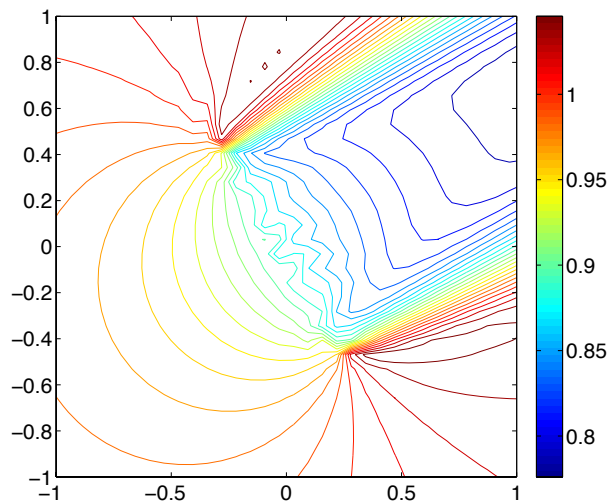


discrete Dirac, Gaussian

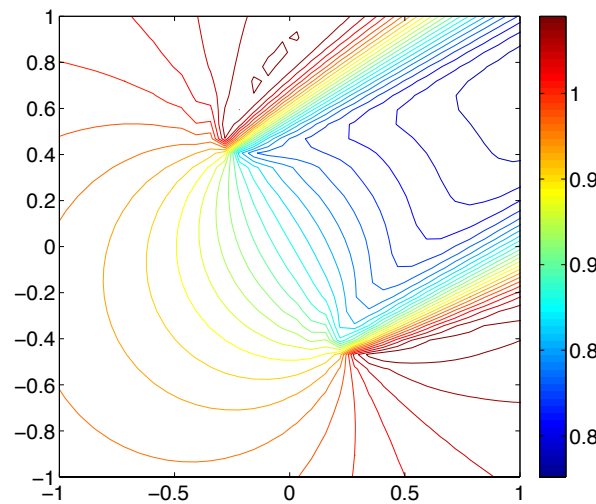
2D actuator disk



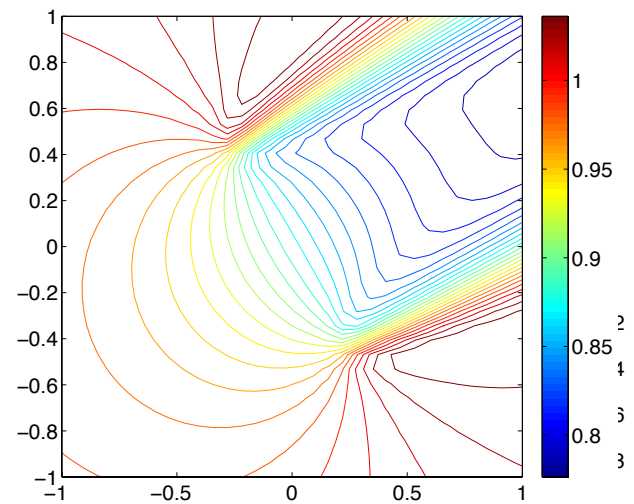
2D actuator disk



no correction

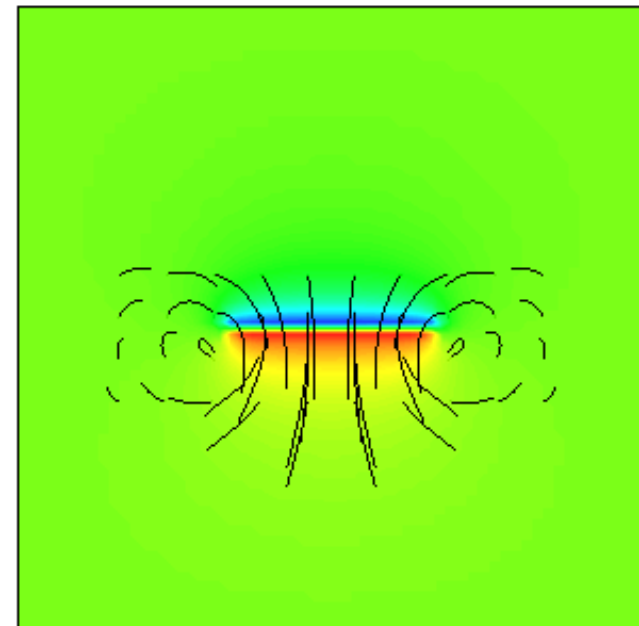
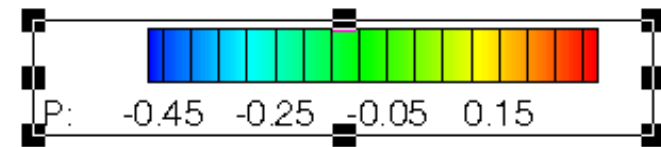
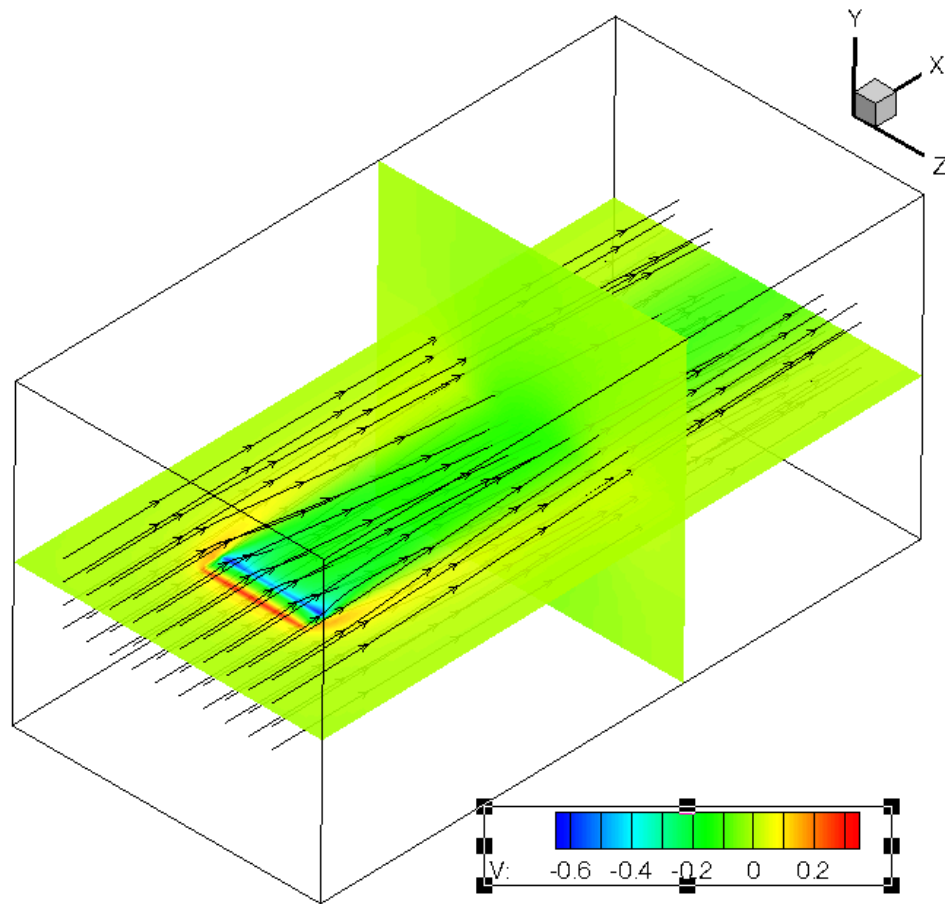


IAM



discrete Dirac (Gaussian)

3D wing



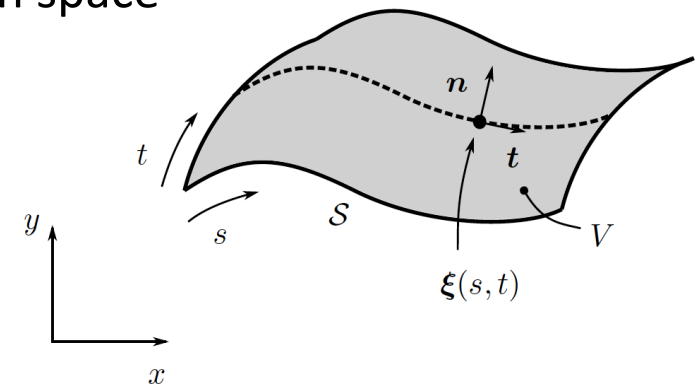
Moving actuators

- Integral form in space *and* time

$$\left[\int_{\Omega} \mathbf{u} \, d\Omega \right]_{t^n}^{t^{n+1}} = \int_{t^n}^{t^{n+1}} (\text{conv} + \text{diff} + \text{press}) \, dt + \int_{t^n}^{t^{n+1}} \mathbf{F}(t) \, dt$$

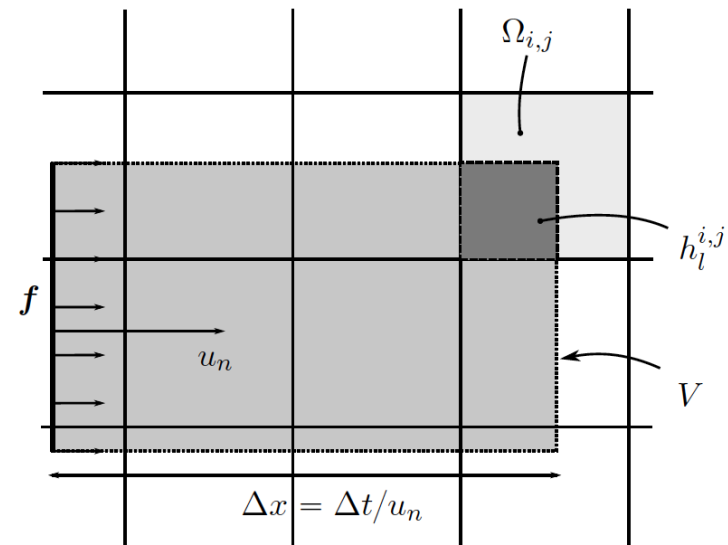
$$\int_{t^n}^{t^{n+1}} \mathbf{F}(t) \, dt = \iint_V \frac{\mathbf{f}^b(\mathbf{x})}{|u_n(\mathbf{x})|} \, dV$$

- Integral in time is transformed into an integral in space



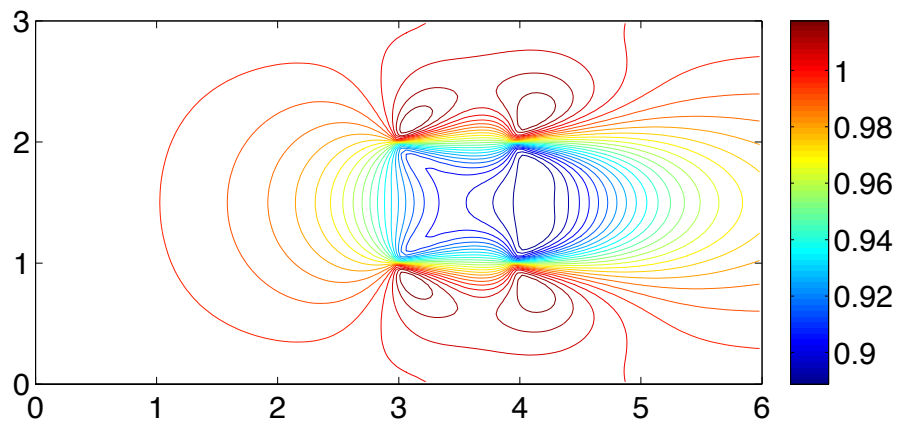
Moving actuators

- Discretization based on $\int_{t^n}^{t^{n+1}} \mathbf{F}(t) dt = \iint_V \frac{\mathbf{f}^b(\mathbf{x})}{|u_n(\mathbf{x})|} dV$
- A finite volume carries a force contribution based on intersectional area
- Total momentum is conserved in a discrete sense
- For general $\mathbf{f}^b(\mathbf{x})$ and $u_n(\mathbf{x})$ we need numerical quadrature method
- We can take much larger time steps

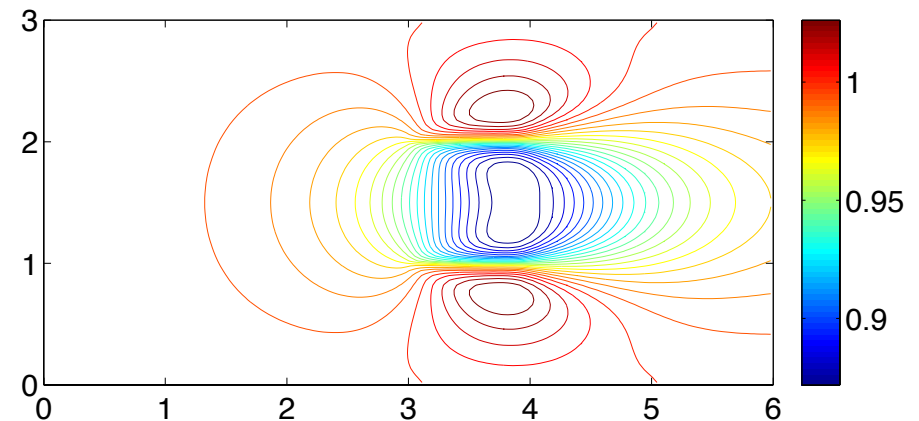


Moving actuators

- Classical time discretization, e.g.:
$$\int_{t^n}^{t^{n+1}} \mathbf{F}(t) dt \approx \frac{1}{2} \Delta t (\mathbf{F}(t^n) + \mathbf{F}(t^{n+1}))$$
- Comparison of new method with classical method; one time step



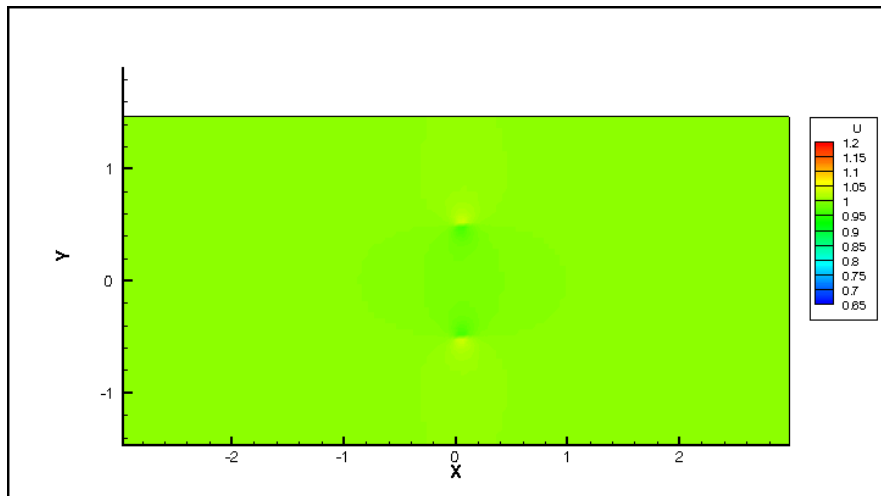
classical



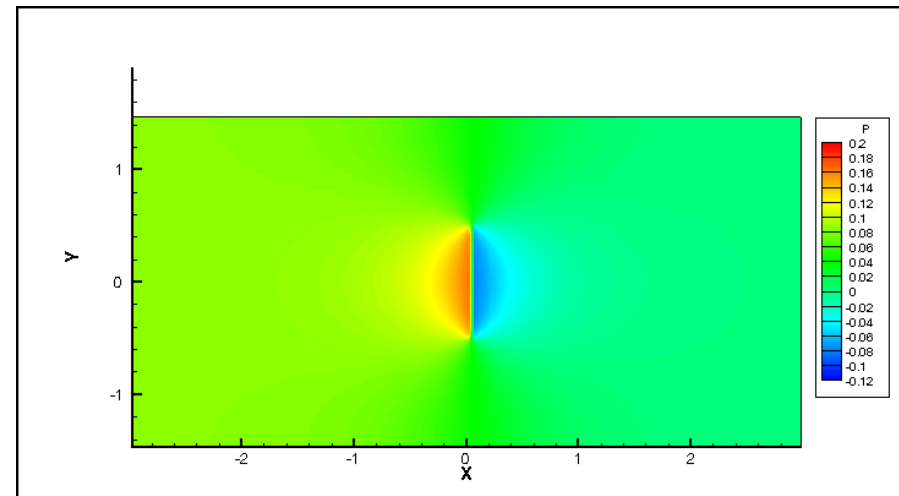
new

Moving actuators

- A **translating** actuator disk with prescribed motion and uniform loading



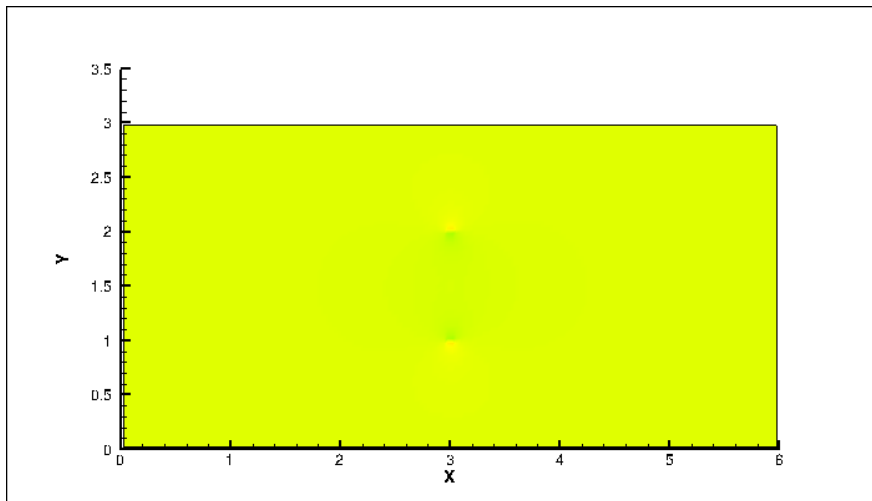
velocity



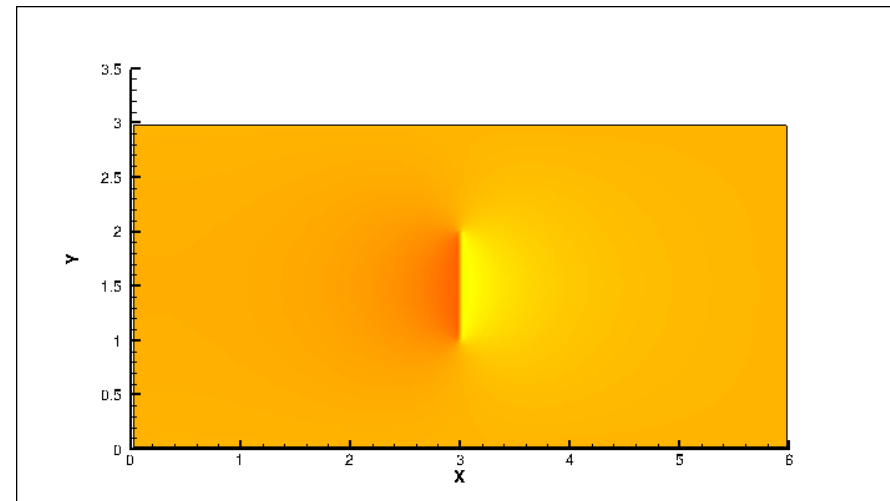
pressure

Moving actuators

- A **rotating** actuator disk with prescribed motion and uniform loading



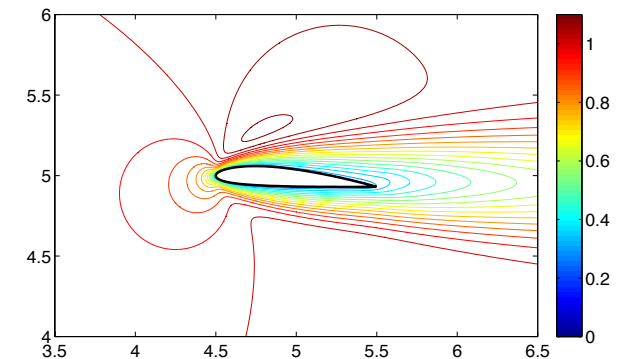
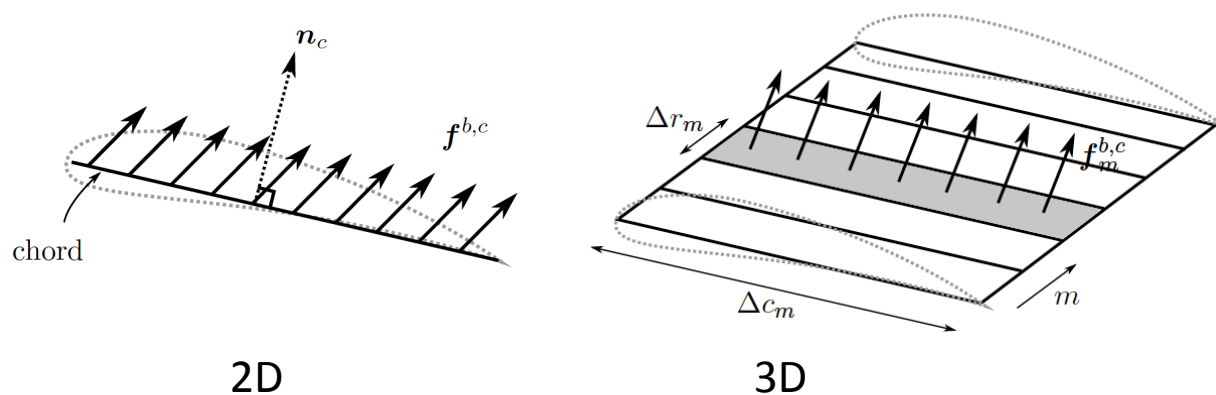
velocity



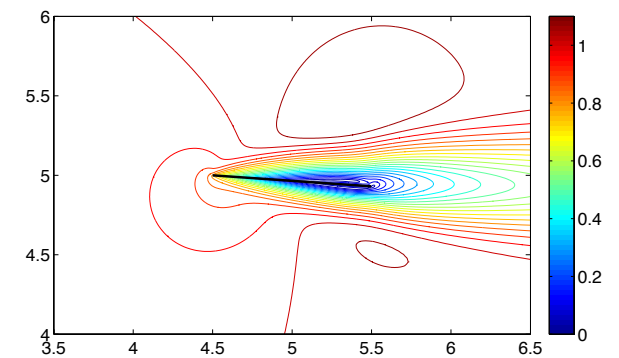
pressure

A general framework

- Current actuator line: 'point' force in 2D, 'line' force in 3D
- A new actuator line model: distribute lift and drag over chord line:
 - Forces are associated with surface
 - Actuator line model is a special case of actuator surface on coarse meshes



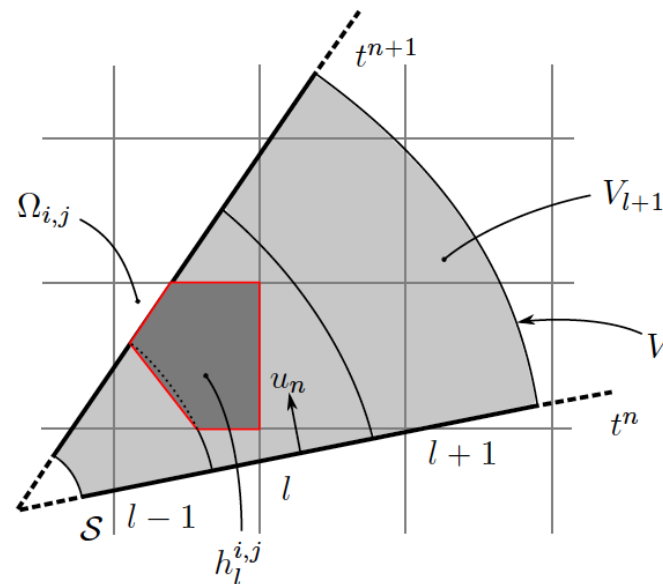
Actuator surface: C_p and C_f



New actuator line: CL and CD

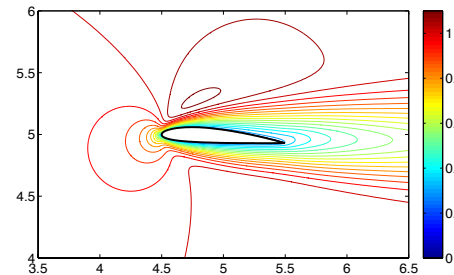
A general framework

- Actuator disk follows from actuator line for large time steps

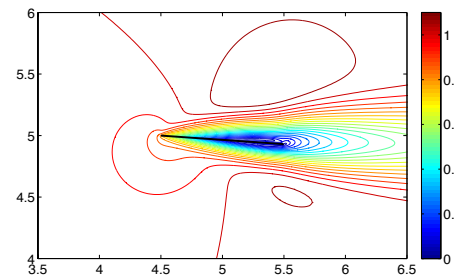


A general framework

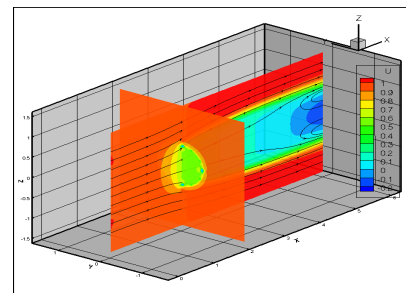
- Actuator surfaces



- Actuator 'line'
(actuator surface with uniform loading)



- Actuator disk



coarser model
OR
coarser mesh

coarser model
OR
larger time step

Conclusions

- Immersed actuator method (IAM):
 - Sharp interface treatment
 - Jump discontinuities in discretization
 - No discrete Dirac functions
- Moving actuators
 - Discretization based on swept area
 - Large time steps allowed
- General framework
 - Actuator surface -> line -> disk



Thank you for your attention

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