

PYRENA: Pyrolysis
equipment for new
approaches in circulating
fluidised bed catalytic
pyrolysis for better bio-oil as
precursor for fuels and
chemicals

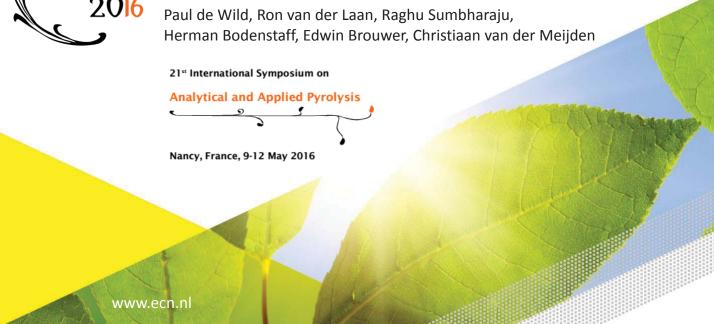
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#### **PYRENA**



**PYR**OLYSIS EQUIPMENT FOR **N**EW **A**PPROACHES in circulating fluidised bed catalytic pyrolysis for better bio-oil as precursor for fuels and chemicals





# Catalytic fast pyrolysis

### Goal(s)

- Improve pyrolysis oil quality regarding its application as a (precursor for) transportation fuels (lower O, less acidic, less unstable, less water, etc.)
- Change pyrolysis oil composition to facilitate the production of value-added chemicals and/or groups of chemicals from the crude liquid product(s)

# Challenges

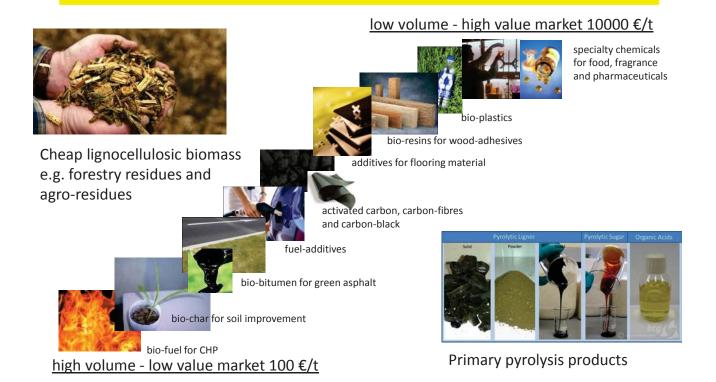
- Low organic yield (low carbon efficiency)
- Unfavourable economics due to high operating costs (feedstock, expensive catalysts) and relatively low value of the liquid product → low price fossil oil!

#### Our approach

- Combine the production of better bio-(fuel)oil with recovery of specific chemicals (e.g. acids, phenolics, anhydrosugars, etc.)
- Research is supported by techno-economic assessments



# Applications for bio-oil and its fractions



### **ECN**

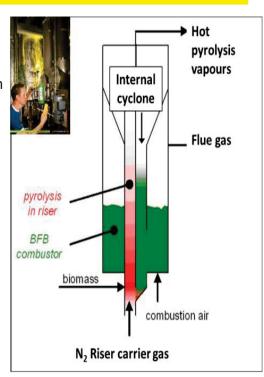
# PYRENA fast pyrolysis

#### Integrated reactor system:

- EF pyrolysis (riser) BFB combustor (annulus)
- 1-5 kg/hr, T up to 900°C, continuous operation
- Thermal pyrolysis (no catalysts)
- Ex-situ pyrolysis (downstream catalyst)
- In-situ pyrolysis (catalyst in combustor bed), suitable for continuous catalyst regeneration
- In-situ and ex-situ combined....

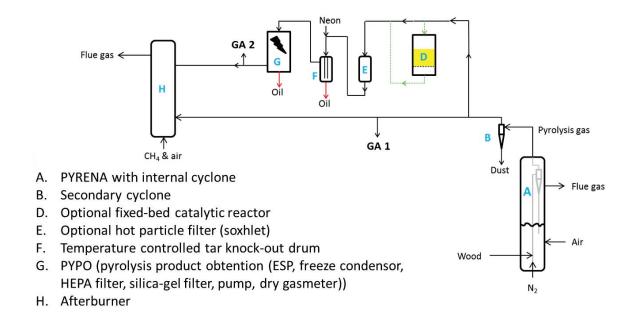
# Pyrolysis oil recovery

 Condensation train with 4°C gas cooler, ambient temperature ESP, -30°C cooler





# PYRENA process flow diagram



GA1, GA2: gas analysis points, including a presample system



#### **PYRENA**

# Advantages

- Compact integrated design
- Autothermal operation via char combustion
- Lower fluidisation gas flow rate (riser) when compared to CFB
- Continuous catalyst regeneration, combination in-situ ex-situ catalysis
- Pyrolysis combustion and pyrolysis gasification possible
- Production of larger bio-oil samples for further evaluation / application trials
- Scale-up possibilities

### Challenges

- Compact integrated design
- Start-up; adjusting proper hydrodynamics



# Fast pyrolysis experiments

#### Materials

- − Softwood: Rettenmaier Lignocel grade 9: 0.9 − 1.1 mm sawdust from selected conifers
- Hybrid poplar fines < 0.5 mm (from Idaho National Lab. US; for Round Robin test)</li>
- Wheat straw fines < 0.5 mm (from Idaho National Lab. US; for Round Robin test)</li>



Ash content at 550°C:

Softwood: 0.5 wt% Poplar: 3.3 wt% Straw: 16 wt%

- Bed material: silica sand 60 200 μm
- In-situ catalysis: alkali metal-based, powder 80 -140 μm



# Fast pyrolysis experiments

### Pyrolysis and sampling conditions

- Feedstock intake 1 3 kg/hr, 500 520°C, 1 atm, N<sub>2</sub> fluidization gas
- Catalyst: biomass ratio ~6, contact time ~seconds, hold-up in combustor ~1 hr
- Overall hot vapour residence time 2-3 sec
- Fractionated pyrolysis oil collection via 4°C gas cooler, ESP and -30°C freeze condenser
- Non catalytic experiments: after collection samples are back-mixed (ultrathurrax)









# IEA-T34 Fast pyrolysis Round Robin: **#ECN** non-catalytic results poplar and wheat straw

# Poplar

- 64% oil (22% water, 42% organics);
   1-phase oil
- 98% mass balance
   (64% oil, 12% gas, 22% char)

#### Wheat straw

- 44% oil (24% water, 20% organics);
   2-phase oil
- 82% mass balance
   (44% oil, 9% gas, 29% char)







# Round Robin analysis results

	Poplar	Wheat straw
Density [g/cm³]	1.149	1.026
Viscosity @ 20°C [cSt]	25.4	n/a
Viscosity @ 50°C [cSt]	5.9	n/a
Aging: Viscosity @ 20°C [cSt]		n/a
Aging: Viscosity @ 50°C [cSt]		n/a
Water content [%]	31.4	n/a
TAN [mg KOH/g]	83.3	n/a
Ash content in oil @ 775°C [%]		
Carbon C [%]	39.2	n/a
Hydrogen H [%]	8.3	n/a
Nitrogen N [%]	0.1	n/a
Py-Lignin [%]	11.75	10.61
Solids [%]		
Sodium Na [ppm]	2.2	10.6
Potassium K [ppm]	16.6	725.3
Magnesium Mg [ppm]	7.3	82.6
Calcium Ca [ppm]	28.5	445.3
Sulphur [ppm]	87.1	922.1
GPC [g/mol]	1555	2296
Dispersity	3.39	3.950

Measured by:

Thünen Institute of Wood Research, Germany (Dr. Dietrich Meier) Incomplete analysis of wheat straw oil due to phase separation

#### Conclusion:

Results representative for proper fast pyrolysis!

PYRENA suitable for FP!



# Preliminary catalytic results with softwood

#### General observations

- Successful experiment with stable pyrolysis behaviour regarding temperatures, pressures and flows → stable hydrodynamics
- Experiment duration 3 hrs at ~1.2 kg/hr feedstock intake
- Acceptable mixing of sand with catalyst; acceptable loss of catalyst
   (<< 5% of the original per hour); mainly dust and fines</li>
- Very active catalyst converts most biomass to gases, water and coke
- No decline in catalyst activity (continuous regeneration seems to work!)

### Product yields (feedstock a.r.)

- 30 - 40% total liquid yield, ~7 - 8% organics

Fraction 1 (gas cooler) : 31%, 5% org (25%O)
 Fraction 2 (ESP) : 2.3%, 2% org (13%O)
 Fraction 3 (freeze cooler) : 1%, 0.3% org (30%O)

- 20 30% non-condensable gases
- 30 40% char/coke



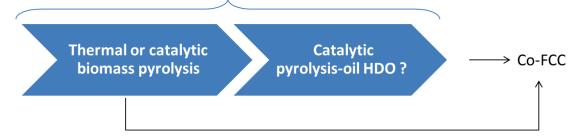


### Techno-economic evaluation

#### TEE to provide input for socio-economic assessment

- Goal of the catalytic pyrolysis is to produce a bio-oil suitable as FCC co-feed
- Modelling with input data from literature and from PYRENA experiments
- Comparison of benchmark route (thermal pyrolysis HDO) with catalytic route (catalytic pyrolysis – (HDO)) to check the effect of a dedicated fast pyrolysis catalyst on the subsequent (need for a) HDO treatment.

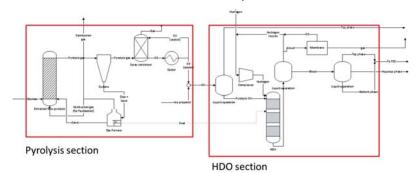
System boundaries modelling





# Approach TEE

- 300 kton/a (dry) biomass (softwood), 8000 hrs operation, CFB pyrolysis
- Comparison thermal pyrolysis → catalytic HDO vs catalytic pyrolysis (ZSM5)
- TP→HDO based on exp data, CP on literature data
- Construction of model (Excel) to calculate mass- and energy balances from both exp and literature data (Mercader, 2010, Paasikallio et al., 2014)
- Economics: estimation of CAPEX, OPEX and economic margin



PYROLYSIS OIL UPGRADING FOR CO-PROCESSING IN STANDARD REFINERY UNITS PROEFSCHRIFT ter verkrijging van de graad van doctor aan de Universiteit Twente, op gezag van de rector magnificus, prof.dr.H. Brinksma, volgens besluit van het College voor Promoties in het openbaar te verdedigen op vrijdag 12 november 2010 om 16.45 uur door Ferran de Miguel Mercader geboren op 12 december 1981

te Balsareny, Spanje

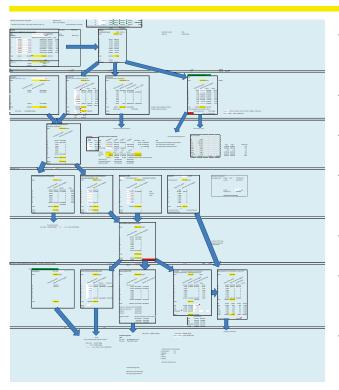
Cite this: Green Chem., 2014, 16, 3549

Product quality and catalyst deactivation in a four day catalytic fast pyrolysis production run†

Ville Paasikallio,\*\* Christian Lindfors,\* Eeva Kuoppala,\* Yrjö Solantausta,\* Anja Oasmaa,\* Jani Lehto\* and Juha Lehtonen



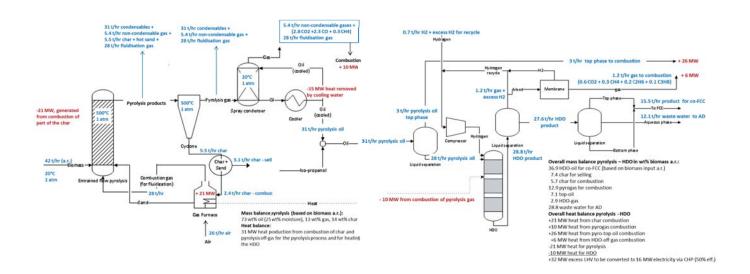
# Modelling approach



- Feedstock input data
- Thermal pyrolysis
- Pyrolysis oil stabilising
- Pyrolysis oil fractionation and hydrodeoxygenation
- Intermediate HDO-oil
- HDO-oil fractionation
- Co FCC feed



# Mass- and energy balance



M & E balance for thermal pyrolysis → hydrodeoxygenation



# Preliminary TEE results

Parameter	Thermal pyrolysis → hydrodeoxygenation	Catalytic pyrolysis (ZSM5 catalyst)
Mass & energy balance		
Organic oil product yield (a.r.) for co-FCC	36.0 wt%	16.5 wt%
O content in the oil	22.6 wt%	21.5 wt%
Lower heating value	31 MJ/kg	29 MJ/kg
Gas yield (a.r.)	15.4 wt%	18.7 wt%
Char yield (a.r.)	12.8 wt%	24.0 wt%
Excess energy yield (e.g. for electricity and/or steam)	32 MW	51 MW
Economics		
Economic margin @ 100 \$/t for wood and 44 \$/b for crude oil	- 6 M€/a	- 3 M€/a
Approximate CAPEX	100 M€	70 M€
Wastes		
Waste water yield (a.r.)	28 wt%	41 wt%



# Conclusions / outlook

### PYRENA suitable for (catalytic) fast pyrolysis

- First promising results in IEA Round Robin collaboration
- Recently: successful functional thermal pyrolysis and in-situ catalytic pyrolysis tests with softwood after several adaptations

# Approach to produce "better" bio-oil

- Combine in-situ with ex-situ catalysis
- Recover bio-oil in fractions → ensure direct phase separation to remove water
- Use lower (< 500°C) pyrolysis temperature in combination with somewhat longer solid and vapour residence times to improve final product stability
- Use reactive riser gas (e.g. steam, H<sub>2</sub>, CO, CO<sub>2</sub>,..)

# Techno-economics

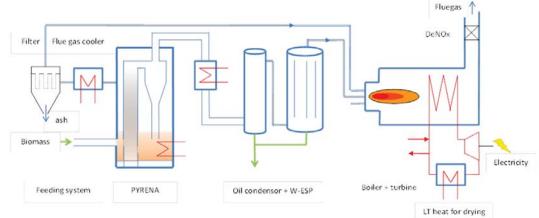
– Presently, both TP→HDO and CP do not seem to be economically feasible at the current market prices for wood and crude oil, → chemicals as money maker?





# Thank you for your attention!

#### Questions and more information: dewild@ecn.nl



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