

# Spatial variation in porosity and permeability of the Rupel Clay Member in the Netherlands

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## Abstract

The spatial distribution of porosity and permeability of the Rupel Clay Member is of key importance to evaluate the spatial variation of its sealing capacity and groundwater flow condition. There are only a limited number of measured porosity and permeability data of the Rupel Clay Member in the onshore Netherlands and these data are restricted to shallow depths in the order of tens of metres below surface. Grain sizes measured by laser diffraction and SediGraph® in samples of the Rupel Clay Member taken from boreholes spread across the country were used to generate new porosity and permeability data for the Rupel Clay Member located at greater burial depth. Effective stress and clay content are important parameters in the applied grain-size based calculations of porosity and permeability.

The calculation method was first tested on measured data of the Belgian Boom Clay. The test results showed good agreement between calculated permeability and measured hydraulic conductivity for depths exceeding 200 m.

The spatial variation in lithology, heterogeneity and also burial depth of the Rupel Clay Member in the Netherlands are apparent in the variation of the calculated permeability. The samples from the north of the country consist almost entirely of muds and as a consequence show little lithology-related variation in permeability. The vertical variation in permeability in the more heterogeneous Rupel Clay Member in the southern and east-southeastern part of the country can reach several orders of magnitude due to increased permeability of the coarser-grained layers.

**Keywords:** permeability, porosity, Rupel Clay

## Introduction

Quantitative knowledge of the subsurface is a prerequisite for assessing and understanding its storage and energy resource potential, resource producibility and environmental impact. Fine-grained sedimentary rocks such as the Rupel Clay Member may be barriers for fluid flow, where fluids include water, oil or gas. Porosity and permeability are of key importance in this respect. The focus of this paper is on porosity and, especially, permeability of the Rupel Clay Member. The Oligocene Rupel Clay Member (also known as Boom Clay) is part of the Rupel Formation. The current burial depth of the Rupel Clay Member varies from close to the surface to about 1500 m (Fig. 1; Vis et al., 2016). The marine sediments of the Rupel Formation were deposited in the southern part of the North Sea Basin. The formation includes three members, from bottom to top: the sandy Vessem

Member, Rupel Clay Member and sandy Steensel Member. The Rupel Clay Member consists of clays that become more silty towards the base and top of the Member. Vis et al. (2016) provide a detailed description of the Rupel Clay Member based on new grain-size analysis data, and interpretation thereof in relation to the geological setting of the Rupel. Texturally, the Rupel Clay Member includes muds, sandy muds and to a lesser extent muddy sands. Vis et al. demonstrate that the Rupel Clay Member shows a spatial variation in lithological composition related to the depositional environment of the sediments: sediments are generally finer-grained and show less vertical variation in the northern Dutch onshore corresponding to a more distal part of the palaeo basin and are coarser-grained and show more vertical heterogeneity in the southern and eastern onshore corresponding to the palaeo basin margin. They subdivide the member into three subunits based on grain-size characteristics: the lower

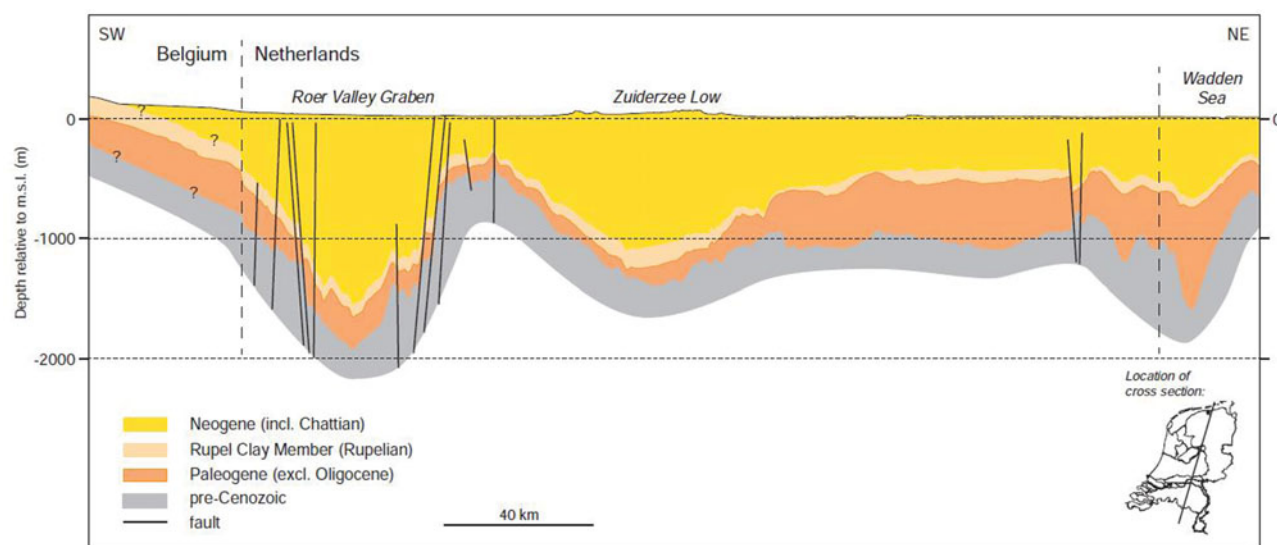


Fig. 1. North-south cross-section showing the variation in burial depth of the Rupel Clay Member (from Vis et al., 2016).

subunit shows a fining upward trend, the middle subunit is finest-grained and the upper subunit shows a coarsening upward trend.

Porosity and permeability or hydraulic conductivity measurements of the Rupel Clay Member in the subsurface of the onshore Netherlands are limited and these measurements are restricted to shallow depths in the order of tens of metres below surface (Rijkers et al., 1998; Wildenborg et al., 2000; Vis & Verweij, 2014). In the northwestern part of Belgium, however, the Boom Clay has been studied extensively for more than 30 years, especially at the Mol investigation site (the High-Activity Disposal Experiment (HADES) underground research facility), which has been constructed in the middle part of the Boom Clay at 223 m depth (Yu et al., 2013). Clay samples from boreholes at Mol and other locations in NW Belgium were used for hydraulic conductivity measurement through laboratory experiments, and *in situ* tests were performed to determine the hydraulic conductivity under undisturbed conditions (Wemaere et al., 2008; Yu et al., 2011).

The grain sizes measured in samples of the Rupel Clay Member taken from boreholes spread across the Netherlands (Fig. 2; Vis et al., 2016) were used to generate new porosity and permeability data for the Rupel Clay Member located at greater burial depth. The published measured hydraulic conductivity data from the Belgium Boom Clay could be used to test and select appropriate input parameters for the grain-size based calculation methods.

### Factors influencing mud porosity and permeability

Muds mostly comprise sediments of fraction  $<63 \mu\text{m}$ , i.e. mostly consisting of a clay fraction ( $<2 \mu\text{m}$ ) and a silt fraction ( $2 \mu\text{m}$ –

$<63 \mu\text{m}$ ). In general, depositional porosities of muds are high, the more so for the clay-rich muds, reaching magnitudes of 80–90% (e.g. Aplin & Macquaker, 2011). Porosity decreases with increasing burial depth. At shallow depths of  $<2 \text{ km}$  (at temperatures  $<70^\circ\text{C}$ ) porosity reduction is mainly due to mechanical compaction driven by the increase of effective stress. Compressibility of mud, and therefore its rate of compaction, is strongly influenced by grain size: finer-grained muds have higher depositional porosities, but their rate of compaction is higher (Yang & Aplin, 2004; Aplin & Macquaker, 2011). In addition, clay mineralogy influences compressibility and compaction. For example, Mondol et al. (2007) demonstrated with experimental mechanical compaction of clay mineral aggregates that coarse-grained kaolinite is more compressible than finer-grained smectite. The clay mineralogy of the Rupel Clay Member consists of a suite of different clays, including kaolinite, smectite, illite and interstratified clay minerals (Koenen & Griffioen, 2014). At a certain porosity, clay-rich mudstones have smaller pore sizes than silt-rich mudstones (Schlömer & Krooss, 1997; Dewhurst et al., 1998, 1999).

Permeability closely relates to pore size and pore-size distribution. Schneider et al. (2011) showed that mudstone permeability increases with a decrease in clay fraction due to the development of a dual-porosity system, where large pore throats between silt grains that act as high-permeability pathways are preserved in addition to small pores within the clay matrix. Just like porosity, permeability of mudstones is also strongly controlled by their grain size, grain-size distribution, and mineralogy. At a given porosity, vertical permeabilities vary over orders of magnitude (Neuzil, 1994; Reece et al., 2012; Casey et al., 2013), while clay-rich mudstones have lower permeabilities than clay-poor ones. This porosity-permeability relation as a function of clay content in fine-grained sediments is consistent with findings of Daigle & Screatton (2015).



Fig. 2. Location of sampled boreholes for grain-size analysis in the Netherlands. The following sampled boreholes were used to calculate porosity and permeability: northern area (BUR-01, LWO-02, GRD-01, ESG-01, EMO-01, NNE-07); southwest and western area (B48G0159, B49G0191, B49G0959, B50H0373); and eastern and southeastern area (B41G0024, B46C0478, B52E0114).

## Database

Grain-size measurements from 107 samples of the Rupel Clay Member from 13 boreholes in the Netherlands were used to

calculate porosity and permeability. The boreholes are listed in Tables 1–3 in Appendix 1, and Figure 2 shows the location of the boreholes. The sampling and grain-size measurement procedures are described in Vis et al. (2016). Grain size was



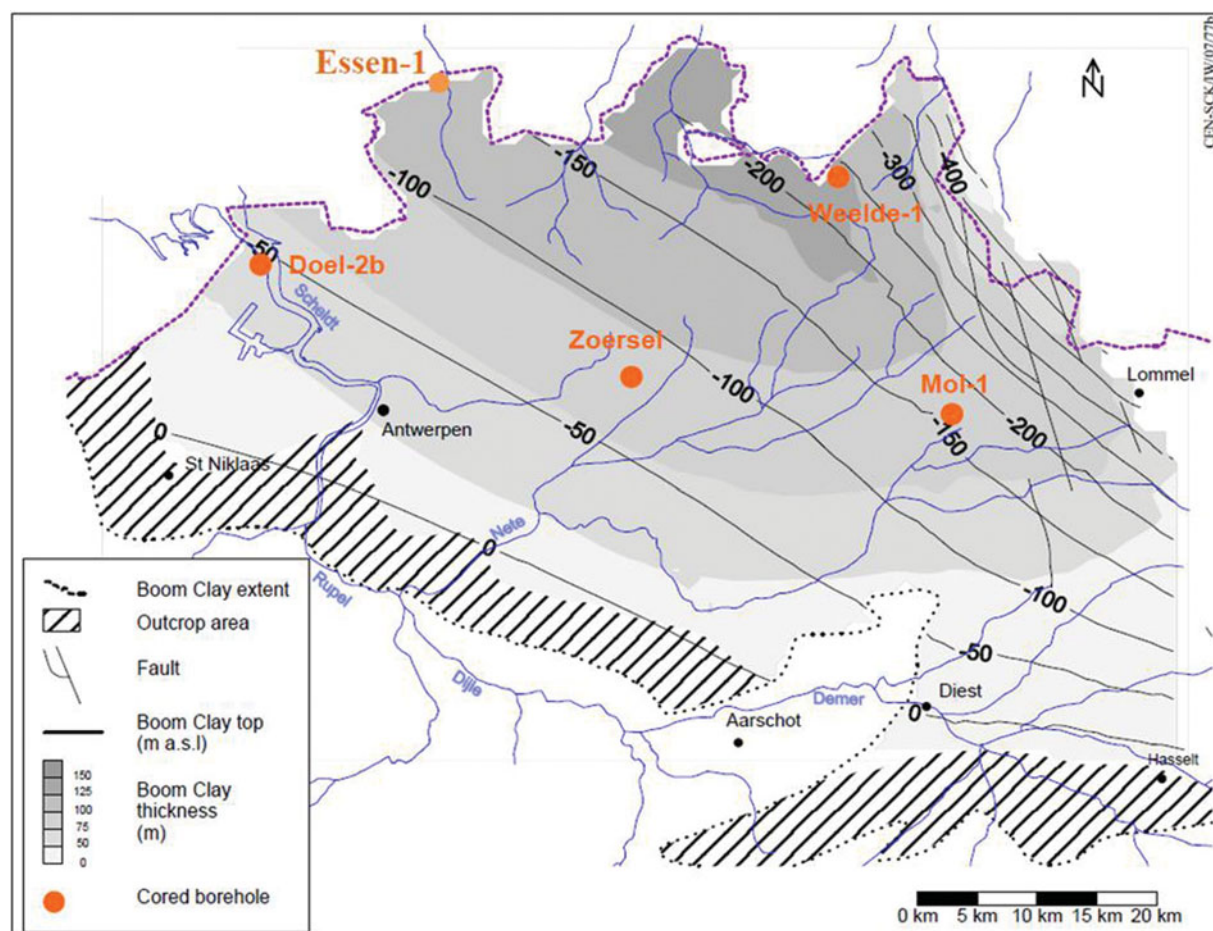


Fig. 3. Location of sampled boreholes and distribution of the 'Boom Clay' in NW Belgium (from Yu et al., 2013, after Wemaere et al., 2008).

measured by Qmineral bvba in Belgium ([www.qmineral.com](http://www.qmineral.com)), using both laser diffraction (low-angle laser light scattering) and SediGraph® (X-ray measurements). The Excel spreadsheet program GRADISTAT8 (Blott & Pye, 2001) was used to analyse the measured grain-size data (Vis et al., 2016). The grain-size measurements of the Rupel Clay Member carried out by two different methods provided the opportunity to compare the clay size measurements of both methods.

Published measured hydraulic conductivity and grain-size data of the Boom Clay at four borehole locations (Mol-01, Zoersel, Weelde-01, Doel-2b) in Belgium (Yu et al., 2011) were used to test the grain-size based method for calculating porosity and permeability. Figure 3 shows the location of these boreholes.

## Methodology

Luijendijk & Gleeson (2015) provided an overview and comparison of grain-size based equations to calculate porosity and permeability developed for sand-clay mixtures using experimental and field datasets. The grain-size based equations discussed are not exclusively for application to muds (grain-size fraction

mostly  $<63\ \mu\text{m}$  and sand content  $<10\%$ ). Yang & Aplin (2004, 2010) developed equations specially designed to calculate mud porosity and vertical permeability, respectively. These equations were selected to calculate porosity and vertical permeability using the grain-size analysis data from mud samples derived from the Rupel Clay Member. Yang & Aplin (2004) used mudstone samples from the North Sea and Gulf of Mexico to describe the mechanical compaction and associated decrease in porosity of mudstones. The relatively shallow sampling depths of the Rupel Clay Member in the Netherlands (21–672 mTVDss (metres true vertical depth below ground surface)) are well within the realm of mechanical compaction. The porosity–permeability equation of Yang & Aplin (2010) was used to calculate permeability. Yang & Aplin derived their permeability equation based mainly on marine mudstones, using more than 300 samples, most of them from the North Sea and Gulf of Mexico. The Yang & Aplin (2004, 2010) equations include clay content and effective stress as important parameters.

In order to test the applicability of the calculation method for the Rupel Clay Member, we compared the permeability based on measured hydraulic conductivity of the Belgian Boom Clay at four borehole locations (Yu et al., 2011) with the calculated permeability using the Yang & Aplin (2004, 2010)

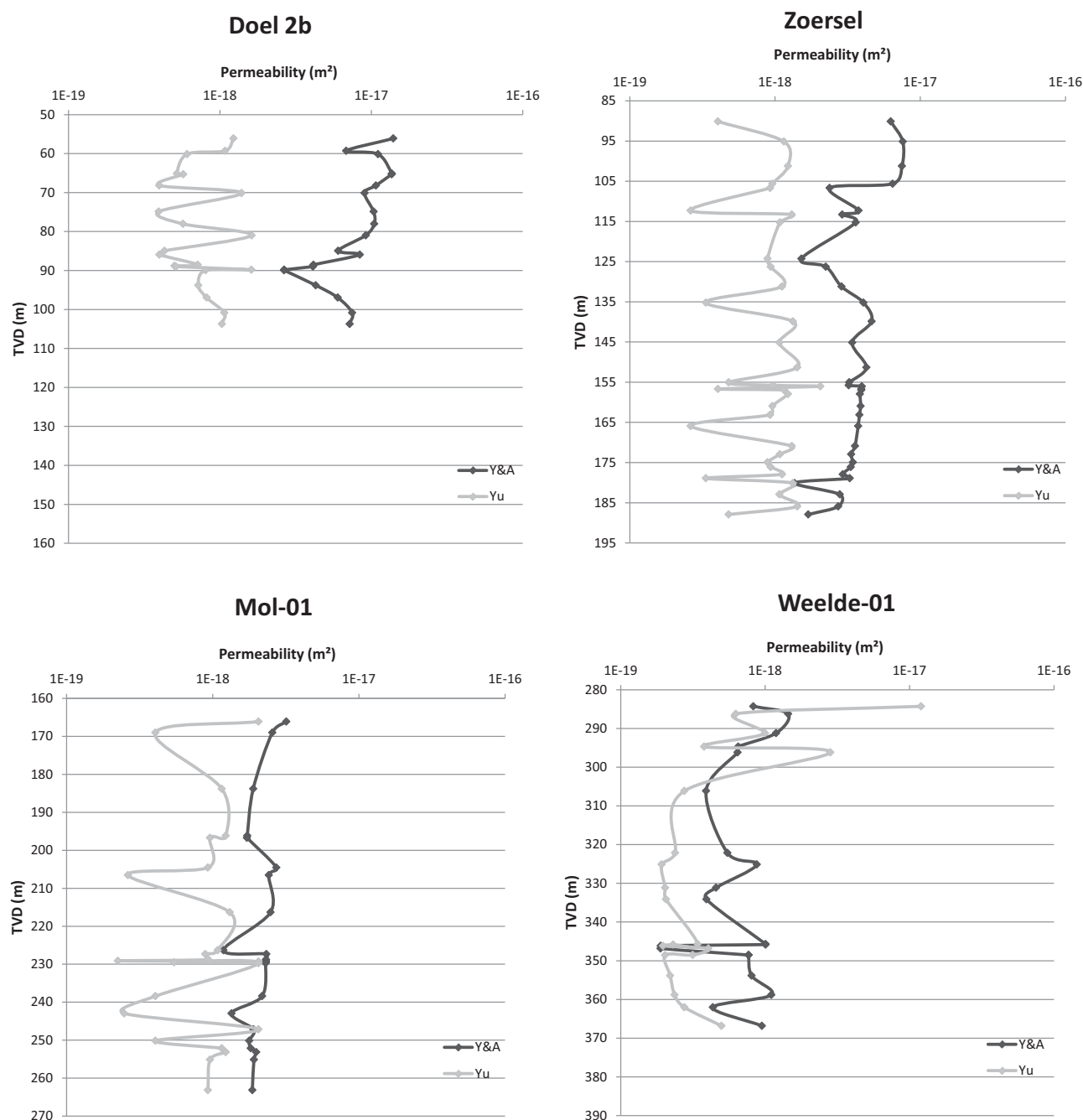


Fig. 4. Cross plots showing measured and calculated permeability of the 'Boom Clay' versus depth at four borehole locations in NW Belgium (see Fig. 3 for location of the boreholes) (modified after Imborechts, 2014 and Verweij et al., 2014). Published measured hydraulic conductivity and grain-size data of the Boom Clay (Yu et al., 2011) were used to derive the measured vertical permeability ('Yu') and the calculated vertical permeability ('Y & A'), respectively.

equations for published measured clay size data from the Boom Clay (Yu et al., 2011) (Fig. 4). Figure 4 shows that the difference between calculated and measured permeability decreases with depth. The largest difference is observed for samples from Doel-2b from depths of <100 m. At depths exceeding 200 m there is a slight overestimation of permeability of less than one order of magnitude.

The clay content is a very important input parameter in the equations. As stated above, the grain sizes of the Rupel Clay

Member were measured by two different methods (laser diffraction and Sedigraph). The results with respect to clay percentage were found to vary strongly depending on the measurement and analysis technique used (Vis et al., 2016). According to Konert & Vandenberghe (1997), the <8  $\mu\text{m}$  grain-size fraction defined by laser techniques corresponds to a grain size of <2  $\mu\text{m}$  defined by classical pipette analysis. They proposed to use the measured fraction smaller than 8  $\mu\text{m}$  (using laser diffraction) as representing the clay fraction, i.e. representing a grain size

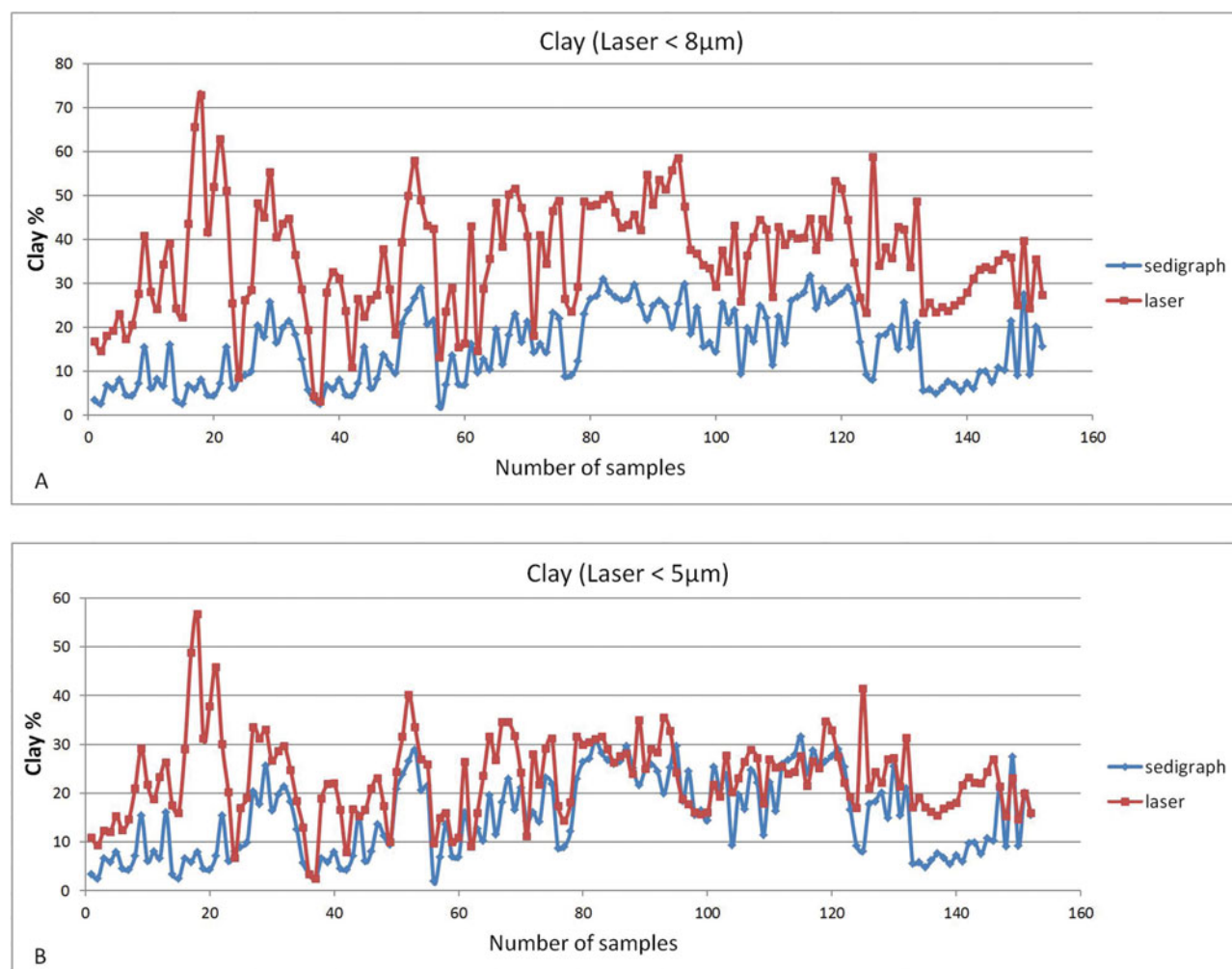


Fig. 5. (A) Comparison of grain-size fraction of  $<8\ \mu\text{m}$  resulting from laser diffraction measurements with the standard grain size for clay ( $<2\ \mu\text{m}$ ) measured with the Sedigraph. (B) Comparison of grain-size fraction of  $<5\ \mu\text{m}$  resulting from laser diffraction measurements with the standard grain size for clay ( $<2\ \mu\text{m}$ ) measured with the Sedigraph. (From Imberechts, 2014.)

smaller than  $2\ \mu\text{m}$ . Based on grain-size measurements of 146 samples from the Rupel Clay Member at 17 borehole locations, Imberechts (2014) investigated which grain size measured with the laser diffraction method corresponds best with the clay fraction of the Rupel Clay Member determined with the Sedigraph. Different grain-size fractions of the laser diffraction measurements, ranging from 2 to  $8\ \mu\text{m}$ , plotted together with the standard clay grain size of  $2\ \mu\text{m}$  of the Sedigraph measurements, showed that the best agreement was found for laser diffraction grain-size measurement of  $5\ \mu\text{m}$  and a Sedigraph measurement of  $2\ \mu\text{m}$  (Fig. 5). Figure 5 shows that the laser grain-size fraction  $<8\ \mu\text{m}$  overestimates the Sedigraph clay fraction of  $2\ \mu\text{m}$ . Imberechts also compared porosity and permeability calculations using Sedigraph clay % ( $<2\ \mu\text{m}$  with laser clay %  $<5\ \mu\text{m}$  and laser clay %  $<8\ \mu\text{m}$ ). The cross plots of calculated porosity and permeability vs depth for the different boreholes showed that in general the porosity and permeability decreases with depth for the Sedigraph and the two laser clay fractions, and that only for about 50% of the boreholes does

the laser clay %  $<5\ \mu\text{m}$  show a better fit with the Sedigraph clay %  $<2\ \mu\text{m}$ .

The calculation of the porosity and permeability, using the Yang & Aplin (2004, 2010) equations was applied to those samples of the Rupel Clay Member that are texturally characterised as mud.

Given the results of Imberechts (2014) and published variations in the measured clay percentages depending on the technique used (Konert & Vandenberghe, 1997; Buurman et al., 2001; Vis et al., 2016), we performed the calculation of porosity and permeability of the mud samples for the following 'clay fraction' measured by laser diffraction and analysed by GRADISTAT8 software (Blott & Pye, 2001), i.e. fraction of grain size  $<8\ \mu\text{m}$  (corresponding to laser-measured fraction of clay + very fine silt + fine silt). The laser diffraction measurements were selected because laser diffraction is the most used method for measuring grain sizes in the Netherlands and calculations based on these measurements allow more direct comparison with older and future permeability calculations.

The porosity and permeability for samples characterised as sandy mud or muddy sand were calculated by conventional lithology-dependent porosity–depth and porosity–permeability relations. The porosity equation is a porosity–depth relation for mechanical compaction based on the conventional Athy's law, and the applied porosity–permeability relation is the multi-point model (Hantschel & Kauerauf, 2009).

## Results

The results of the porosity and permeability calculations are presented in Appendix 1 and Figure 6. The vertical permeability values of the mud part of the Rupel Clay Member at depths of >400 m are all in the range of  $10^{-19}$  m<sup>2</sup> (corresponding to a vertical hydraulic conductivity of  $10^{-12}$  m s<sup>-1</sup>).

The spatial variation in lithological composition of the Rupel Clay Member is reflected in variation in its permeability. Samples of the boreholes in the northern part of the Netherlands (LW0-02, GRD-01, EMO-01; and seven out of eight samples of ESG-01) are all muds and show the least vertical variation in permeability (Fig. 6). For example, the vertical permeability of the Rupel Clay Member in GRD-01 varies between  $5.0\text{E-}19$  and  $6.9\text{E-}19$  m<sup>2</sup> over a depth interval of 448–569 m. The four low permeability outliers for their depth of measurement (Fig. 6) are associated with a high clay content of about 55–70%. In both the east-southeastern and the southwest-southern areas the 'mud' part of the Rupel Clay Member is overlain and/or underlain by coarser-grained sediments: the vertical variation in permeability over the Rupel Clay Member reflects this heterogeneity (Fig. 6). For example, the vertical permeability of the Rupel Clay Member in B52E0114 (east-southeastern area) varies between  $4.6\text{E-}14$  m<sup>2</sup> and  $1.6\text{E-}19$  m<sup>2</sup> over a depth interval 381–524 m, and that in B50H0373 (southern area) varies between  $6.0\text{E-}17$  m<sup>2</sup> and  $7.4\text{E-}19$  m<sup>2</sup> over a depth interval of 325–470 m. The highest permeability for the depth of measurement is related to very high sand contents: for example, the two samples with highest permeability have sand contents of 76.3 and 82.2%. It should be realised by comparing permeability of muds and coarser-grained textures, that different calculation methods were used to estimate the permeability of the mud and the coarser-grained muddy-sand and sandy-mud parts of the Rupel Clay Member.

Spatial variation in the calculated vertical permeability of the Rupel Clay Member also reflects differences in its burial depth in addition to differences in lithology (Fig. 6). The calculated permeability for the samples in the southwest and southern area also clearly shows this influence. The calculated vertical permeability for mud samples decreases from  $7.7\text{E-}17$  m<sup>2</sup> at a very shallow depth of 21 m (B48G0159),  $1.2\text{E-}17$  m<sup>2</sup> (B49G0191; 82 m),  $5.8\text{E-}18$  m<sup>2</sup> (B49G0959; 129 m), to  $9.2\text{E-}19$  m<sup>2</sup> at 442 m (B50H0373).

## Discussion

There are a number of uncertainties involved in the application of the Yang & Aplin (2004, 2010) equations for calculating porosity and permeability of the mud part of the Rupel Clay Member:

- An important uncertainty concerns the clay content to be used. The two methods, laser diffraction and Sedigraph, that were used to measure grain sizes of the samples produce different results for the clay content. Several authors have shown that clay content is underestimated by the laser-diffraction method (Konert & Vandenberghe, 1997; Buurman et al., 2001). This is confirmed by the present study. There is, however, uncertainty about the magnitude of the underestimation. Here we followed Konert & Vandenberghe (1997) and used clay <8 µm measured by laser diffraction.
- The permeability model of Yang & Aplin (2010) is based on the assumption of homogeneity of the mud sample. The spatial lithological heterogeneity in muds at cm to m scale is not taken into account in the model. Heterogeneity at this scale also affects the pore size distribution and as a consequence its permeability to a greater or lesser extent (Hildenbrand, 2003; Drews, 2012; Hemes et al., 2013). Heterogeneity at this scale occurs in the Rupel Clay Member, especially in the southern and eastern parts of the country. In this study the vertical permeability was calculated for sample scale only. On a larger scale, the grain-size data and associated permeability showed that the Rupel Clay Member exhibits layering on a member scale. The Rupel Clay Member is probably also anisotropic to a greater or lesser extent. This was also demonstrated by vertical and horizontal hydraulic conductivity measurements performed on the Belgian Boom Clay. The measurements showed that the horizontal conductivity, at formation scale, can be 5–60 times higher than the vertical ones (Wemaere et al., 2008).
- Yang & Aplin (2010) reported that for their database (300 samples of marine mudstones, mostly from the North Sea and Gulf of Mexico) an uncertainty of magnitude in permeability at a given porosity is one order of magnitude. The mud samples from the Rupel Clay Member belong to one system, in contrast to the samples from the Yang & Aplin (2010) study. It is currently not known if this more homogeneous sample set reduces the uncertainty in calculated permeability for the Dutch mudstones.
- The porosity and permeability has been calculated using effective stress values related to current burial depth. Burial history has not been taken into account. If previous deeper burial of the Rupel Clay has occurred at a certain location, this may have led to overcompaction of the clay. Such a condition is known/expected to occur in the SW of the Netherlands where the Rupel Clay Member is at very shallow depths (Vis et al., 2016). Hitherto no influence of past



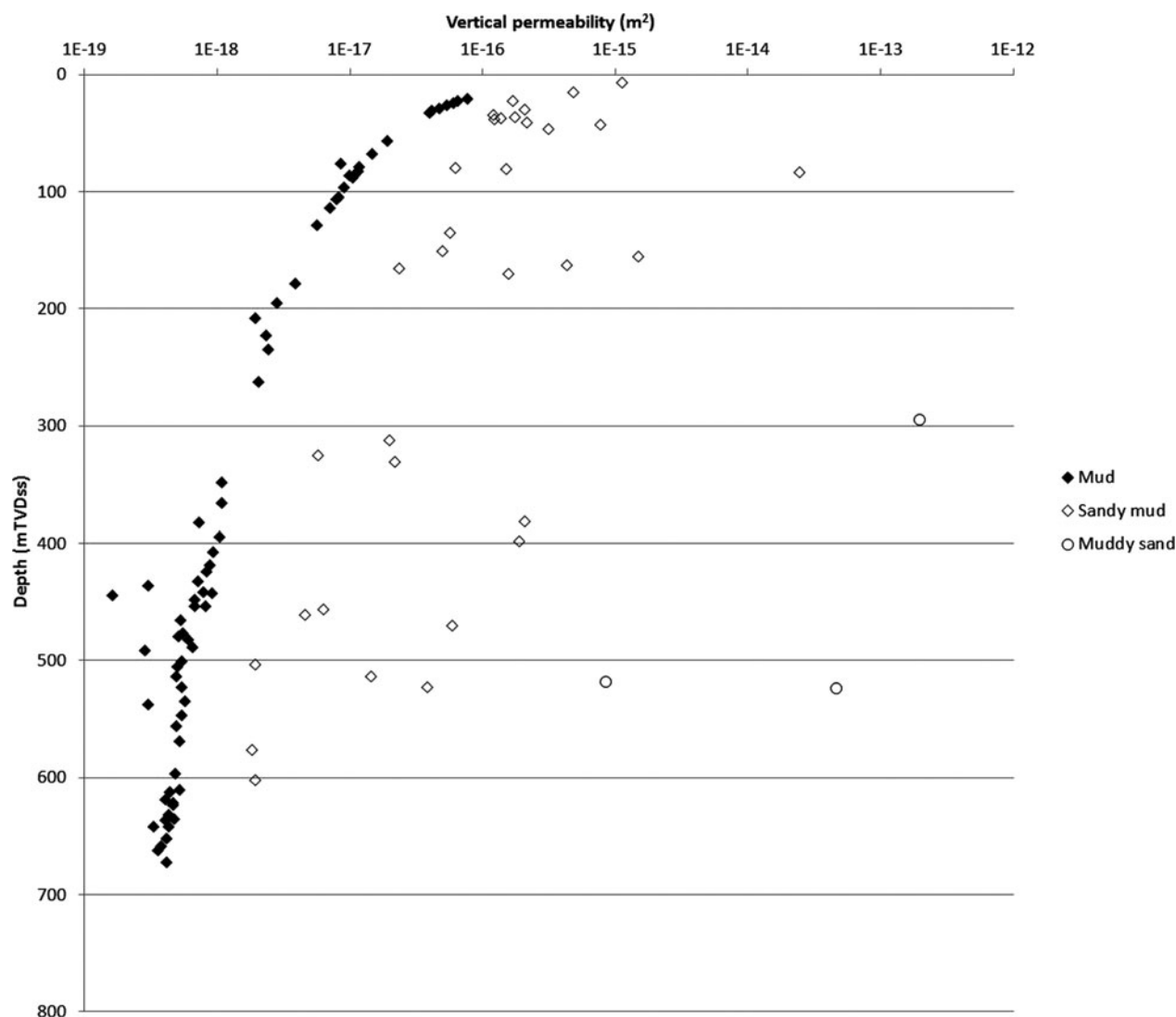


Fig. 6. Cross plot of calculated vertical permeability versus depth for samples of mud, sandy mud and muddy sand of the Rupel Clay Member (see Appendix 1 for the calculated values).

glacial loading has been identified for Paleogene mudrocks in the northern part of the Netherlands (Kooi, 2000).

- The calculation method does not take into account the influence of variation in mineralogy. Koenen & Griffioen (2014, 2016) analysed samples from the Rupel Clay Member across the Netherlands to characterise geochemistry and mineralogy. They found that the clay mineralogy of the Rupel Clay Member consists of a suite of different clays, including kaolinite, smectite, illite and interstratified clay minerals.

In order to obtain insight into the applicability of the calculation method for the Rupel mud samples, the results of calculations were compared with measured hydraulic conductivity values for the Belgian Boom Clay. This comparison indicated that for a depth of >200 m there is a slight overestimation of permeability of less than one order of magnitude. The calcu-

lated vertical permeability of the mud part of the Rupel Clay Member in the Netherlands probably also slightly overestimates its real value.

## Conclusions

Comparison of the permeability based on measured hydraulic conductivity of the Belgian Boom Clay at four borehole locations (Yu et al., 2011) with the calculated permeability using the Yang & Aplin (2004, 2010) equations for published measured clay size data from the Boom Clay (Yu et al., 2011) showed that the calculated permeability slightly overestimates measured permeability by less than one order of magnitude for burial depths exceeding 200 m. An important uncertainty in the application of the calculation method concerns the clay content to be used from laser diffraction grain-size measurements.



The calculated porosity and vertical permeability of the Rupel Clay Member provide, for the first time, insight into these key properties at depths beyond a few tenths of a metre.

The spatial variation in lithology, heterogeneity and also burial depth is apparent in the variation of the calculated vertical permeability using the grain-size analyses of the samples of the Rupel Clay Member. The samples from the north of the country consist almost entirely of muds with calculated vertical permeability of less than  $8.3 \times 10^{-19} \text{ m}^2$  ( $8.3 \times 10^{-12} \text{ m s}^{-1}$ ) (calculated using clay + very fine silt + fine silt % from laser diffraction measurements). The vertical variation in permeability in the more heterogeneous Rupel Clay Member in the southern and east-southeastern part of the country can reach several orders of magnitude due to increased permeability of the coarser-grained sandy-mud and muddy-sand layers.

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## Appendix 1: Calculated porosity and vertical permeability of the Rupel Clay Member

Table 1. Calculated porosity and vertical permeability of the Rupel Clay Member in the northern area. Figure 2 shows the borehole locations.

NORTHERN AREA												
Well name	Top NMFRC <sup>a</sup> (mTVDss) <sup>a</sup>	Bottom NMFRC <sup>a</sup> (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural group	Clay ( $< 2 \mu\text{m}$ ) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability (m <sup>2</sup> )	Hydraulic conductivity (m s <sup>-1</sup> )
BUR-01	570.8	646.06	XV-1	576.1	sandy mud	6.6	80.6		12.8	25	1.9E-18	1.9E-11
			XV-2	641.6	mud			46.1	4.9	34	3.4E-19	3.4E-12
LWO-02	590.69	674.51	XI-1	597	mud			38.5	6.1	32	4.9E-19	4.9E-12
			XI-2	619	mud			42.1	4.0	33	4.1E-19	4.1E-12
			XI-3	637	mud			40.0	1.9	32	4.2E-19	4.2E-12
GRD-01	446.07	570.81	VIII-1	447.8	mud			46.1	0.3	38	6.8E-19	6.8E-12
			VIII-2	453.8	mud			45.0	0.0	37	6.9E-19	6.9E-12
			VIII-3	482.3	mud			45.2	0.1	37	6.1E-19	6.1E-12
			VIII-4	500.3	mud			46.5	0.2	37	5.4E-19	5.4E-12
			VIII-5	513.8	mud			47.3	0.2	37	5.0E-19	5.0E-12
			VIII-6	522.8	mud			43.5	0.3	35	5.5E-19	5.5E-12
			VIII-7	534.8	mud			40.2	3.8	33	5.8E-19	5.8E-12
			VIII-8	546.8	mud			40.9	2.5	34	5.5E-19	5.5E-12
			VIII-9	555.8	mud			42.9	2.4	34	5.0E-19	5.0E-12
			VIII-10	568.8	mud			39.3		32	5.3E-19	5.3E-12
ESG-01	602.75	689.96	XII-1	601.7	sandy mud	6.6	79.7		13.7	25	2.0E-18	2.0E-11
			XII-2	611.7	mud			40.4	7.5	32	4.5E-19	4.5E-12
			XII-3	621.7	mud			36.7	8.3	30	4.7E-19	4.7E-12
			XII-4	631.7	mud			38.8	4.8	31	4.4E-19	4.4E-12
			XII-5	641.7	mud			37.7	2.2	31	4.3E-19	4.3E-12
			XII-6	651.7	mud			37.8	1.1	31	4.2E-19	4.2E-12
			XII-7	661.7	mud			42.1	0.1	32	3.6E-19	3.6E-12
			XII-8	671.7	mud			35.0	1.4	29	4.2E-19	4.2E-12
EMO-01	604.72	668.27	XIV-1	611	mud			31.9	6.3	28	5.3E-19	5.3E-12
			XIV-2	623	mud			36.1	5.9	30	4.8E-19	4.8E-12
			XIV-3	636	mud			33.6	4.1	29	4.8E-19	4.8E-12
			XIV-4	658	mud			40.4	0.5	32	3.9E-19	3.9E-12

Table 1. Continued.

NORTHERN AREA												
Well name	Top NMFRCA (mTVDss) <sup>a</sup>	Bottom NMFRCA (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural group	Clay ( $< 2 \mu\text{m}$ ) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability (m <sup>2</sup> )	Hydraulic conductivity (m s <sup>-1</sup> )
NNE-07	427.98	538.64	XIII-1	432	mud			46.5	0.9	38	7.2E-19	7.2E-12
			XIII-2	441.5	mud			41.7	3.8	36	8.0E-19	8.0E-12
			XIII-3	453	mud			38.1	2.6	34	8.3E-19	8.3E-12
			XIII-4	465	mud			50.4	0.4	40	5.4E-19	5.4E-12
			XIII-5	476.5	mud			48.6		39	5.5E-19	5.5E-12
			XIII-6	488.5	mud			41.8	3.5	35	6.6E-19	6.6E-12
			XIII-7	503.5	sandy mud	9.1	79		11.9	26	2.0E-18	2.0E-11
			XIII-8	513.5	sandy mud	9.5	63.1		27.4	25	1.5E-17	1.5E-10
			XIII-9	522.5	sandy mud	8.6	58.1		33.3	24	3.9E-17	3.9E-10
			XIII-10	537	mud			56.1	0.5	41	3.1E-19	3.1E-12

<sup>a</sup>NMFRCA: Rupel Clay Member.<sup>b</sup>mTVDss: metres true vertical depth below ground surface.



Table 2. Calculated porosity and vertical permeability of the Rupel Clay Member in the southwest and southern area. Figure 2 shows the borehole locations.

SOUTHWEST & SOUTHERN AREA												
Well name	Top NMFRCA (mTVDss) <sup>b</sup>	Bottom NMFRCA (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural rroup	Clay (<2µm) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability (m <sup>2</sup> )	Hydraulic conductivity (m s <sup>-1</sup> )
B48G0159	20.01	43.09	IX-1	21	mud			51.8	1.7	60	7.7E-17	7.7E-10
			IX-2	23	mud			45.2	1.7	56	6.5E-17	6.5E-10
			IX-3	25	mud			50.6	1.5	59	6.1E-17	6.1E-10
			IX-4	27	mud			48.7	5.2	57	5.4E-17	5.4E-10
			IX-5	29	mud			53.4	0.7	60	4.8E-17	4.8E-10
			IX-6	31	mud			55.6	1.5	60	4.2E-17	4.2E-10
			IX-7	33	mud			44.6	0.4	54	4.1E-17	4.1E-10
			IX-8	35	sandy mud	6.0	83.3		10.7	52	1.2E-16	1.2E-09
			IX-9	37	sandy mud	5.2	82.4		12.4	52	1.8E-16	1.8E-09
			IX-10	39	sandy mud	4.6	85.3		10.1	52	1.2E-16	1.2E-09
			IX-11	41	sandy mud	4.1	81.4		14.5	51	2.2E-16	2.2E-09
			IX-12	43	sandy mud	7.2	69.8		23.0	50	7.8E-16	7.8E-09
B49G0191	79.12	84.37	X-1	79.9	sandy mud	5.9	83.4		10.7	48	6.4E-17	6.4E-10
			X-2	80.9	sandy mud	5.2	80.2		14.6	48	1.5E-16	1.5E-09
			X-3	81.9	mud			40.8	9.9	47	1.2E-17	1.2E-10
			X-4	82.9	sandy mud	9.5	48.1		42.4	45	2.5E-14	2.5E-07
			X-5	84.7	mud			34.3	7.4	43	1.1E-17	1.1E-10
B49G0959	73.54	174.5	VII-1	75.8	mud			16.8	6.9	31	8.6E-18	8.6E-11
			VII-2	87.8	mud			39.0	3.0	46	1.1E-17	1.1E-10
			VII-3	106.8	mud			32.3	1.5	40	8.0E-18	8.0E-11
			VII-4	113.3	mud			43.8	2.5	47	7.2E-18	7.2E-11
			VII-5	128.8	mud			46.1	0.8	47	5.8E-18	5.8E-11
			VII-6	155.3	sandy mud	6.0	55		39.0	38	1.5E-15	1.5E-08
			VII-7	162.8	sandy mud	4.2	64.2		31.6	38	4.4E-16	4.4E-09
			VII-8	170.3	sandy mud	5.4	69.2		25.4	38	1.6E-16	1.6E-09

Table 2. Continued.

SOUTHWEST & SOUTHERN AREA												
Well name	Top NMFC <sup>a</sup> (mTVDss) <sup>b</sup>	Bottom NMFC <sup>a</sup> (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural rroup	Clay (<2µm) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability (m <sup>2</sup> )	Hydraulic conductivity (m s <sup>-1</sup> )
B50H0373	319.49	472.02	III-1	324.7	sandy mud	6.4	80.3		13.3	31	5.8E-18	5.8E-11
			III-2	330.7	sandy mud	7.2	69.2		23.6	29	2.2E-17	2.2E-10
			III-3	348.2	mud			46.0	5.2	40	1.1E-18	1.1E-11
			III-4	365.7	mud			42.9	2.7	38	1.1E-18	1.1E-11
			III-5	382.2	mud			52.0		42	7.4E-19	7.4E-12
			III-6	394.2	mud			38.4	1.6	35	1.1E-18	1.1E-11
			III-7	407.2	mud			41.3	1.6	36	9.4E-19	9.4E-12
			III-8	424.2	mud			42.4	1.7	37	8.5E-19	8.5E-12
			III-9	442.2	mud			34.6	4.0	32	9.2E-19	9.2E-12
			III-10	455.7	sandy mud	6.2	76		17.8	27	6.4E-18	6.4E-11
			III-11	469.7	sandy mud	5.1	62.6		32.3	26	6.0E-17	6.0E-10

<sup>a</sup>NMFC: Rupel Clay Member.<sup>b</sup>mTVDss: metres true vertical depth below ground surface.

Table 3. Calculated porosity and vertical permeability of the Rupel Clay Member in the east and southeastern area. [Figure 2](#) shows the borehole locations.

EAST SOUTHEASTERN AREA												
Well name	Top NMFRC <sup>a</sup> (mTVDss) <sup>b</sup>	Bottom NMFRC <sup>a</sup> (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural group	Clay ( $<2\mu\text{m}$ ) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability ( $\text{m}^2$ )	Hydraulic conductivity ( $\text{m s}^{-1}$ )
B41G0024	1.97	107.91	VI-1	6.75	sandy mud	5.0	70.4		24.6	52	1.1E-15	1.1E-08
			VI-2	14.75	sandy mud	6.1	75.7		18.2	52	4.9E-16	4.9E-09
			VI-3	22	sandy mud	9.4	78.9		11.7	53	1.7E-16	1.7E-09
			VI-4	29.5	sandy mud	4.7	81.5		13.8	52	2.1E-16	2.1E-09
			VI-5	37.25	sandy mud	6.4	81.2		12.4	51	1.4E-16	1.4E-09
			VI-6	46.25	sandy mud	10.1	71		18.9	49	3.2E-16	3.2E-09
			VI-7	56.75	mud			45.8	3.7	52	1.9E-17	1.9E-10
			VI-8	67.75	mud			36.6	7.6	46	1.5E-17	1.5E-10
			VI-9	78.25	mud			47.8	1.9	51	1.2E-17	1.2E-10
			VI-10	86.25	mud			49.0	1.1	51	1.0E-17	1.0E-10
			VI-11	96	mud			44.8	3.8	49	9.1E-18	9.1E-11
			VI-12	104.75	mud			38.0	4.7	44	8.4E-18	8.4E-11
B46C0478	132.69	345.61	V-1	135.3	sandy mud	7.2	76.5		16.3	42	5.8E-17	5.8E-10
			V-2	150.3	sandy mud	6.1	77.1		16.8	40	5.1E-17	5.1E-10
			V-3	165.3	sandy mud	4.8	83		12.2	40	2.4E-17	2.4E-10
			V-4	178.3	mud			37.0	4.5	40	3.9E-18	3.9E-11
			V-5	195.3	mud			47.2		45	2.9E-18	2.9E-11
			V-6	208.3	mud			55.3	0.3	49	2.0E-18	2.0E-11
			V-7	222.3	mud			46.6	2.4	44	2.4E-18	2.4E-11
			V-8	234.3	mud			40.6	5.6	40	2.5E-18	2.5E-11
			V-9	262.3	mud			39.9	6.9	39	2.1E-18	2.1E-11
			V-10	294.3	muddy sand	4.2	19.5		76.3	28	2.0E-13	2.0E-06
			V-11	312.3	sandy mud	5.5	73.3		21.2	30	2.0E-17	2.0E-10

Table 3. Continued.

EAST SOUTHEASTERN AREA												
Well name	Top NMFRC <sup>a</sup> (mTVDss) <sup>b</sup>	Bottom NMFRC <sup>a</sup> (mTVDss) <sup>b</sup>	Sample no.	TVDss (m)	GRADISTAT textural group	Clay ( $< 2\mu\text{m}$ ) (%)	Silt (%)	Clay to fine silt (%)	Sand (%)	Porosity (%)	Permeability (m <sup>2</sup> )	Hydraulic conductivity (m s <sup>-1</sup> )
B52E0114	364.7	526.7	II-1	380.95	sandy mud	7.5	52.9		39.6	27	2.1E-16	2.1E-09
			II-2	398.45	sandy mud	7.2	54.2		38.6	27	1.9E-16	1.9E-09
			II-3	418.45	mud			41.4	9.7	36	8.9E-19	8.9E-12
			II-4	436.2	mud			63.3		46	3.0E-19	3.0E-12
			II-5	443.7	mud			70.7		49	1.6E-19	1.6E-12
			II-6	460.35	sandy mud	13.5	70.3		16.2	28	4.6E-18	4.6E-11
			II-7	479.2	mud			49.9	1.9	39	5.2E-19	5.2E-12
			II-8	491.45	mud			60.5	0.4	44	2.9E-19	2.9E-12
			II-9	504.95	mud			47.8		38	5.1E-19	5.1E-12
			II-10	518.45	muddy sand	11.2	31.9		56.9	23	8.4E-16	8.4E-09
			II-11	523.7	muddy sand	3.9	13.9		82.2	23	4.6E-14	4.6E-07

<sup>a</sup>NMFRC: Rupel Clay Member.<sup>b</sup>mTVDss: metres true vertical depth below ground surface.