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J. Buiten and H. Aartsen

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INVESTIGATION INTO NOISE EXPOSURE OF ENGINE ROOM PERSONNEL ABOARD M.S. "TRIDENT AMSTERDAM"

by

J. BUITEN AND ING. H. AARTSEN

Technisch Physische Dienst TNO-TH (Institute of Applied Physics TNO-TH)

Summary

The noise exposure in terms of equivalent continuous sound level L_{eq} of engine room personnel was determined aboard the freighter m.s. "Trident Amsterdam" during ordinary trade voyages by means of two methods: the first by making use of dosimeters, the second by measuring the sound levels in the engine room at 165 positions and the exposure times of the engineers involved for three operating conditions of the ship. The two methods gave results which were in good agreement.

A further conclusion is that a simplified calculation method may offer a reliable alternative for determining the value of $L_{\epsilon 0}$.

1 Introduction

Aboard ships engine room personnel is often exposed to high noise levels during the working hours.

Without any countermeasure this would sooner or later result in hearing impairment for a great percentage of the exposed persons.

Because this has become widely known the personnel involved wear hearing protectors and feel themselves quite safe by doing so. However this may only be expected to be justified for the great majority of the personnel if the sound level, to which the ear is exposed, is lower than 90 dB (A).

The sound level at the position of the ear is the result of the sound level in the environment minus the sound level difference introduced by the ear defender. The maximum permissible level in the environment, e.g. the engine room could be determined if the insertion loss of the ear defender is known.

However, this is less simple than it seems to be because:

- 1. there are many types of protection items
- the sound level difference introduced by a certain protector depends on the physical shape of the wearer's head or ear.

Nevertheless an idea can be obtained of the permissible sound levels, if the investigation is restricted to earmuffs using caps.

The insertion loss (IL) of a great number of earmuffs is given e.g. in [1]. The influence of the wearer on the average value of the IL can be expressed by its standard deviation (s). The average IL may be supposed to be reached for 50% of the wearers. However a greater protection rate is frequently required e.g. 80%. In this case the average IL has to be decreased by the standard deviation. A protection rate of 98% is reached when twice the standard deviation is subtracted from the average IL data. Using the spectrum as may be expected to be typical for engine room noise the attenuation of an earmuff expressed in dB(A) can be calculated. Doing

this for the earmuff with the highest and for the one with the lowest IL given in [1] the following data is obtained:

	ΔL_{A}	$\Delta L_A - s$	$\Delta L_A - 2s$
earmuff 1	32	29	26
earmuff 2	18	13	8

So, starting with the limit of 90 dB(A) at the ears, the highest permissible sound level in the engine room could be within the range 98–119 dB(A), depending on the desired protection rate and on the acoustical properties of the earmuffs used. The lowest level of this range is well below the limit of 110 dB(A) proposed, among others, by the Dutch authorities.

However, the 90 dB(A) limit is valid for a continuous exposure during an eight-hours' working day, 40 hours per week. This is not the case aboard modern ship because it is common practice and required by many authorities, to install a control room if the levels in the engine room exceed 90 dB(A).

So the personnel will only be exposed to high levels during a part of their duty hours. In that case the exposure is not continuous and higher levels, depending on exposure time, are permissible following [2]. When the levels to which a person is exposed vary in relation to time they may be described by a so-called equivalent continuous level (L_{eq}) being the continuous level which would result in the same amount of sound energy as it would be the case for the varying level during the same time.

The aim of the investigation reported in the next chapters was to obtain some insight into the relation between the sound levels existing in the engine room and the $L_{\rm eq}$. Furthermore it would be profitable if the $L_{\rm eq}$ could be calculated from the sound levels and the exposure times. In that case the $L_{\rm eq}$ could be obtained in the future by executing only sound level measure-

ments in the engine room or even be obtained from calculated levels.

However the exposure time is in fact unknown and therefore it was also necessary to obtain this quantity aboard the ship under investigation. Because the measurement of $L_{\rm eq}$ and the determination of exposure times asked a great amount of organisation and accompaniment, the investigation aboard the m.v. "Trident Amsterdam" were used to test the system of data collection and to obtain experience about the necessity of the accompaniment of the measurement $L_{\rm eq}$ during long sailing times.

2 Data of the ship

The measurements were carried out aboard the freighter the m.v. "Trident Amsterdam" during ordinary trade voyages. Some general data of the ship and the propulsion system are:

Length between perpendiculars	156.00 m
Breadth moulded	23.30 m
Depth moulded	12.50 m
Loaded draft	8.26 m
Service speed during measurements	20 knots

Propulsion diesel engine (1):

manufacturer	Schelde Sulzer
type	8 RND – 2 stroke
output	12 MW
speed	125 rpm

Auxiliary diesel engines (3):

manufacturer	Smit - B & W
type	8 T 23 HH - 4 stroke
output	$3 \times 0.72 \text{ MW}$
speed	750 rpm

3 General conditions during the measurements

The operating conditions during the measurements were:

sound pressure level measurements:

at sea : main engine 6 MW at 124 rpm and auxiliary diesel engines no. 2 and 3

in the harbour: auxiliary diesel engines no. 1 and 2.

- equivalent continuous sound level measurements:

at sea : main engine output about 10.5 MW
at 122 rpm and two of the auxiliary

diesel engines; output varying between 150-225 kW each

in the harbour: auxiliary diesel engines no. 2 and 3;

output varying between 150-225 kW each.

4 Measuring equipment

The sound pressure levels were recorded via a 1" microphone, manufactured by General Radio, on magnetic

tape using a recorder manufactured by Kudelski, type Nagra IV SJ.

For determining the equivalent continuous sound levels the 1944-1 noise monitors were worn on duty hours by the persons who were exposed to noise. The measured noise-exposure indexes, which were read with the aid of a 1944-1 noise exposure indicator, were further converted into equivalent continuous levels. The monitor as well as the indicator are manufactured by General Radio.

5 Measuring procedure

5.1 Measurement of sound pressure levels

Surveys of noise measurements have been carried out during two voyages of the ship. On a coastal trip, sailing from Rotterdam to Hamburg, the sound pressure levels were recorded on magnetic tape at a large number of positions in the engine room. Since the noise levels in the harbour and at sea are quite different, measurements were taken under both conditions viz. with only the auxiliary diesel engines in operation and at service speed whereas the propulsion engine was also running.

The measuring positions were chosen at places at which the engineers probably spent a large part of their time and of course at quite a number of places along the route which has to be taken when the watch keeping engineer makes his round through the engine room.

For the determination of the measuring positions the surfaces of the tanktop and platform decks in the engine room were divided into rectangular sections with dimensions of about 1.50×1.50 m. The measuring locations were chosen at 1.65 m perpendicular above the middle of these sections.

The number given to a measurement is composed of seven figures, see the Table in the Appendix, indicating the location of the rectangular section in which the particular data is measured, the operating condition of the ship during the measurements and the quantity of the measured value, the last one only to enable the calculations to be performed with the aid of a computer.

5.2 Measurement of noise doses

During the crossing of the North Atlantic from Hamburg to Baranquilla the equivalent continuous sound levels, $L_{\rm eq}$ to which the engineers during their presence in the engine room are exposed, were measured. Aboard this ship two four-hour watches are kept from 8.00–12.00 hours and from 13.00–17.00 hours, the time between these periods the ship sails with an unmanned engine room except at short periods before arriving and after leaving a harbour.

During a watch the engineer in charge was provided with a noise exposure monitor. From the measurements

and the observations made during the watch the following data were obtained:

- the noise exposure index measured during the round through the engine room
- the duration of the round through the engine room
- the route of the rounds through the engine room
- the arrival times at several positions.

The other available noise-exposure monitors were distributed to the engineers who executed maintenance in the engine room during the mentioned watches. At places where these engineers mainly spent their time the duration of the exposure was measured.

6 Results of measurements and calculations

6.1. Sound pressure level measurements

The recordings have been analysed with a 1/3-octave band-analyser and from the results octave band levels and sound levels-A have been calculated. These data and the NR-numbers which are obtained from the octave band spectra are given in Table 1 of the Appendix. Additionally the sound levels-A calculated for the operating conditions "service speed" and "harbour" are given at the measuring positions on the general arrangements of the Floor and the several platform decks, see the Fig. 1–8 of the Appendix.

At about 1 m from the main engine on deck no. 1 (= Floor) and deck no. 2 the averaged sound level-A is about 95 dB(A) and on deck no. 3: 93 dB(A). In the vicinity of the auxiliary diesel engines the space averaged sound level-A is about 97 dB(A). The highest levels, 100 dB(A), have been measured between two operating auxiliary diesel engines and in the vicinity of

Table 1. Averaged values of the sound levels in dB(A) at various areas in the engine room. Operational condition of the ship: service speed

area	number of measuring positions	average value of sound levels $(\overline{L_A})$	standard deviation	level of the mean-square space averaged A-weighted sound pressure $(L_{\overline{A}})$
deck 1 (floor)	53	94.5	2.7	95.3
deck 2	39	92.6	3.2	93.4
deck 3	42	90.0	4.2	91.8
deck 4	1	88.0	-	88.0
deck 5	5	89.0	2.1	89.4
deck 6	9	87.0	1.3	87.2
deck 7	9	85.6	1.1	85.7
shaft tunnel	4	85.8	1.5	86.0
control room	4	79.8	1.0	79.8
workshop	2	87.0	0	87.0
store	6	77.3	2.9	78.2
deck 1, near				
aux. diesel				
engines	20	97.2	1.7	97.4
decks 1-3	134	92.5	3.9	93.9

the turbocharger. In the control room and in the workshop the averaged sound levels are 80 and 88 dB(A) respectively. In the Tables 1 and 2 a survey of the sound levels averaged per deck is given.

6.2. Noise doses

In the Tables 3, 4 and 5 the results of the noise dose measurements, the $L_{\rm eq}$'s and the exposure times are given. From the routes, the exposure time and the measured sound levels $L_{\rm eq}$'s are calculated, which was only possible with respect to the inspection watches. The results are given in Table 6.

Two different types of $L_{\rm eqm}$ are used in the Tables 3-6: $L_{\rm eqm}$ and $L_{\rm eqs}$. $L_{\rm eqm}$ is the $L_{\rm eq}$ for the time T which equals the exposure time and $L_{\rm eqs}$ where for the time T eight hours is chosen:

$$L_{eq} = 10 \log \left\{ \frac{1}{T} \int_{0}^{T} p^{2}(t) dt \right\}$$
 (1)

where p = rms-value of the sound pressure at the time tT = total time taken into consideration.

When using for T the duration of the measuring period $L_{\rm eq}$ is proportional to the time-averaged energy of the sound, supposing the integration time is sufficiently long. This quantity is used to investigate if space-averaged sound levels can be used in stead of $L_{\rm eq}$.

The calculated $L_{\rm eq}$ are obtained by using the relation

$$L_{\rm eq} = 10\log\left\{\frac{1}{T}\int_{0}^{T} 10^{L_{t}/10} \cdot dt\right\}$$
 (2)

where $L_t = \text{sound level at time } t$ $T = \text{total time } = \sum t_i$.

Table 2. Averaged values of the sound levels in dB(A) at various areas in the engine room.

Operational condition of the ship: in the harbour

area	number of measuring positions	average value of sound levels $(\overline{L_A})$	standard deviation	level of the mean-square space averaged A-weighted sound pressure $(L_{\overline{A}})$
deck 1 (floor)	37	91.3	4.5	93.6
deck 2	19	87.5	2.7	88.3
deck 3	24	83.2	2.6	83.8
deck 4	1	84.0	-	84.0
deck 5	4	81.8	2.1	82.1
deck 6	7	82.3	1.6	82.6
deck 7	9	80.9	0.8	81.0
control room	3	78.0	0.0	78.0
workshop	2	81.5	0.7	81.5
deck 1, near aux. diesel				
engines	16	94.7	4.1	96.1
decks 1-7	101	86.7	5.2	90.3
decks 1-3	80	88.0	5.0	91.1

For the normal watches reported in Table 3, $L_{\rm eq_m}$ could be calculated very precisely because the exposure times during the rounds at each of the measuring positions in the engine room were known (Table 7).

Additionally the L_{eq_m} was calculated using a less fine division e.g. the exposure per deck (Table 6).

For the assessment of the noise exposure in relation to hearing impairment $L_{\rm eq}$ must be known for a period of 8 or 40 hours. The $L_{\rm eq}$ to which an engineer is exposed during an 8-hour working day can be obtained by addition of two $L_{\rm eqs}$ each of which being obtained during a 4-hour watch following the power law

$$L_{\text{eq}_{101}} = 10 \log (10^{L_{\text{eq}_1}/10} + 10^{L_{\text{eq}_2}/10})$$

The L_{eqs} 's given in the Tables 3, 4 and 5 are thus giving

Table 3. Survey of the measured $L_{\rm eq_m}$ and $L_{\rm eq_8}$ in dB(A) to which the watch keeping engineers are exposed during their inspection rounds through the engine room. The integration times used are the round duration time $(\dot{L}_{\rm eq_m})$ and 8 hours $(L_{\rm eq_8})$ respectively.

Operational condition of the ship: service speed

measure- ment no.	round no.	round duration time (min)	total watch keeping time (min)	L_{eq_m} (dB(A))	L_{eq_8} (dB(A))
6	1	25	162	94.8	82.7
9	2	49	250	92.3	83.3
14	3	88	270	95.6	88.5
16	4	21	250	96.8	84.1
26	5	25	135	-	_
27	6	127	240	_	-
31	7	18	250	96.3	83.1
33	8	21	250	94.8	82.5
41	9	20	245	95.0	82.9
45	10	77	260	96.0	88.3
48	11	24	215	98.4	85.8
53	12	60	160	94.4	86.6
56	13	21	120	94.7	82.3
68	14	18	210	94.4	81.5
74	15	84	210	95.1	87.7
83	16	25	210	94.9	83.0
59	17	73	210	94.6	86.7
119	18	19	210	_	-
127	19	57	210	92.6	83.9
128	20	13	210	_	-
133	21	44	255	95.3	85.5
137	22	27	210	95.2	83.1
140	23	57	210	93.4	84.6
144	24	17	210	96.7	83.1
145	25	86	210	95.4	88.1
146	26	22	227	94.5	82.3
147	27	69	180	94.8	86.6
149	28	20	210	95.9	83.0
152	29	66	180	92.8	84.5
157	30	17	210	93.9	81.0
160	31	57	150	92.4	83.5
167	32	23	210	90.5	79.6
172	33	14	201	90.7	78.5
total numb	per n =	33	33	29	29
average va		41.9	210.3	94.6	84.0
standard d	eviation				
s ==		28.8	35.8	1.7	2.5

Table 4. Survey of the measured L_{eq} of engineers who kept watches and executed maintenance in the engine room. Operational condition of the ship: service speed

measure-	exposure time	$L_{\mathrm{eq}_{\mathbf{m}}}$	L_{eq_8}	location where maintenance is
ment no.	(min)	(dB(A))	(dB(A))	executed *
4	165	91.8	82.2	_
5	218	93.9	90.5	-
8	240	91.5	88.5	-
15	265	98.3	95.7	aux. diesel engine
17	220	99.3	95.9	aux. diesel engin
19	215	96.0	92.5	aux. diesel engine
22 23	240 245	94.5 99.4	91.5	-
25	253	98.6	96.5 95.8	aux. diesel engine aux. diesel engine
29	245	94.9	92.0	-
30	290	98.3	96.1	_
32	250	97.0	94.2	_
34	250	98.3	95.5	_
35	185	89.6	85.5	deck 6
36	185	88.8	84.7	deck 6
37	185	94.3	90.2	_
38	200	92.9	89.1	-
39	245	98.9	93.7	_ ,
40	245	87.2	82.0	-
42	120	100.0	94.0	aux. diesel engine
46	240	98.2	95.2	-
47.	260	95.9	93.2	
49	215	98.1	94.6	aux. diesel engine
50	215	100.0	96.5	aux. diesel engine
51 54	240 155	94.7	91.7	- auv dissal sasia
58	120	98.1 97.4	93.2 91.4	aux. diesel engine
60	210	92.2	88.6	_
64	235	90.7	87.6	deck 7
66	235	94.6	91.5	deck 1
69	60	88.8	79.8	deck 1, 2
70	235	95.1	92.0	-
71	235	94.7	91.6	_
72	235	97.2	94.1	_
73	240	94.6	91.6	_
. 75	185	95.9	91.8	deck 1
76	185	96.1	92.0	deck 1
77	180	90.4	86.1	deck 3
129	210	99.4	95.8	aux. diesel engine
130	210	98.1	94.5	aux. diesel engine
131	210	97.9	94.3	aux. diesel engine
134	255	98.8	96.1	main engine
135 138	240 210	97.3 99.1	94.3	main engine
139	210	97.9	95.5 94.3	aux. diesel engine
141	180	98.0	93.7	aux. diesel engine aux. diesel engine
142	180	98.2	93.9	aux. diesel engine
143	180	89.7	85.4	deck 6, 7
150	210	92.4	88.8	deck 3
151	210	91.0	87.4	workshop
153	180	91.7	87.4	workshop
154	180	86.4	82.1	-
155	210	94.2	90.6	-
159	210	90.3	86.7	-
161	155	93.6	88.7	deck 1
162	210	94.0	90.4	deck 1
163	210	88.7	85.1	deck 3
164	210	99.0	95.4	deck 1
	210	99.6	96.0	deck 1
168	210	94.3	90.7	-
170	210	92.6	89.0	_
171	210	95.0	91.4	-
	62 210.5	95.1	91.2	

When the location is not given the maintenance was carried out throughout the entire engine room.

no complete information about the noise exposure because only one four-hour watch was considered whereas the additional duty time, spent in the engine room performing maintenace, was neglected.

7 Discussion of the results

7.1

The highest sound levels measured in the engine room of the m.v. "Trident Amsterdam" appear to be 100 dB(A) (Table 1, Appendix).

During sailing conditions only at tanktop and at the decks 2 and 3 the averaged values of the levels per deck exceed 90 dB(A) (Table 1). For the harbour condition this is only at tantop the case (Table 2). The highest levels occur near the auxiliary diesel engines and in the vicinity of the turbocharger of the propulsion engine. The averaged value of the measured $L_{\rm eq}$ of the inspection watches appears to be 94.6 dB(A), or rounded to the nearest whole decibel: 95 dB(A) (Tables 3 and 9).

The similar values of the calculated data are (rounded) 94 dB(A) which is in good agreement with the measured value. The standard deviations are low for the measured as well as for the calculated data and from the Table 7 it appears that the $L_{\rm eq}$'s deviate very

Table 5. Survey of the measured L_{eq} of engineers who kept watches and executed maintenance in the engine room. Operating condition of the ship: in the harbour

measure- ment no.	exposure time (min)	$L_{eq_{\mathbf{m}}}$ (dB(A))	L_{eq_8} (dB(A))	location where maintenance is executed
10	260.	92.9	90.2	-
11	260	90.9	88.3	entire engine room
12	260	93.6	90.9	deck 1, main engine
13	252	89.4	86.6	_
78	210	94.8	92.1	_
79	210	94.2	90.6	-
81	210	97.3	93.7	deck 2, compressor
88	215	92.5	89.0	entire engine room
89	215	92.7	89.2	deck 1, 2
90	210	91.9	85.9	entire engine room
96	210	91.2	85.2	prop. shaft tunnel
98	240	92.4	89.4	deck 1, 2
101	210	91.7	85.7	deck 3, main engine
102	210	86.5	80.5	entire engine room
104	210	86.2	80.2	workshop
108	240	90.8	84.8	engine room
112	210	89.4	83.4	=
116	210	93.1	87.1	deck 2, location 02/50-51
117	210	90.0	84.0	=
118	210	89.3	83.3	deck 3, location 01/51-54
123	280	92.7	90.3	deck 1, location 01-02/51-54
124	280	90.6	88.3	deck 1, location 01-02/51-54
n =	22			
$\bar{x} =$	228.3	91.6	87.2	
s =	25.4	2.6	3.6	

little from round to round. This is mainly caused by the fact that about 18 minutes of the round duration time of 42 minutes (averaged values, see Table 6) are spent at tanktop, where the highest levels are present.

Also from Table 7 it appears that, from a statistical point of view, it makes little difference (0.3 dB(A)) if the L_{eq} is obtained by using observations about the position of an engineer, made every 30 seconds or less, or by using the exposure time per deck combined with the level of the méan-square space averaged A-weighted sound pressure $L_{\bar{A}}$ per deck (Table 6). The calculated L_{eqs} equals $L_{\bar{A}}$ when the latter is obtained from the sound pressures measured at the three lowest levels in the engine room (93.9 dB(A), see Table 1). This certainly will not be a coincidence but will probably differ slightly from ship to ship.

Table 6. The L_{eq_m} to which watch keeping engineers are exposed during their rounds through the engine room, calculated by using the exposure times per deck and the averaged sound levels $L_{\overline{A}}$ at each of the decks in the engine room; obtained from Table 1.

Operational condition	of	the	ship:	service speed	
-----------------------	----	-----	-------	---------------	--

	time sp at deck			total time at a	calculated			
round	1	2 .	3	6	7	shaft	round	
no.	(floor)		•			tunnel	(min)	(dB(A))
1	12	3 .	10	0	0	0	25	94.0
2	0	32	17	0	0	0 .	49	92.9
3	45	22	15	4	2	0	88	94.1
4	9	4	8	0	0	0	21	93.9
5	5	10	10	0	0	0	25	93.3
6	51	23	35	12	2	4	127	93.5
7	6	8	4	0	0	0	18	93.9
8	7	5	9	0	0	0	21	93.6
9	8	6	6	0	0	0	20	93.4
10	39	23	13	4	2	6	77	94.3
11	13	5	6	0	0	0	24	94.3
12	33	9	9	2	2	5	60	94.0
13	12	3	6	0	0	0	21	94.3
14	9	4	5	0	0	0	18	94.4
15	37	23	16	2	1	5	84	93.8
16	10	7	8	0	0	0	25	93.9
17	42	14	8	2	2	5	73.	94.1
18	6	9	4	0	0	0	19	93.9
19	26	13	10	0	0	8	57	93.6
20	6	4	3	0	0	0	13	94.1
21	18	10	9	2	2	3	44	93.5
22	18	4	5	0	0	0	27	94.6
23	26	12	9	1	2	7	. 57	93.7
24	8	4	5	0	0	0	17	94.1
25	37	20	16	2	2	8	86	93.7
26	12	8	2	0	0	0 .	. 22	94.4
27	31	10	14	5	4	0	69	93.5
28	11	5	4	0	0	0	20	94.3
29	31	17	7	2	2	7	66	93.8
30	8	4	5	0	0	0	17	94.1
31	13	17	16	3	1	7	57	92.9
32	13	4	6	0	0	0	23	94.3
33	5	4	5	0	0	0 .	14	93.8
n =	33	33	33	33	33	33	33	33
$\bar{x} =$	18.4	10.5	9.2	1.24			41.9	93.9
s =	13.9	7.6	6.3	2.40	1.03	2.97 -	28.8	0.4

For the watches which are spent on maintenance the average value of the measured $L_{\rm eq}$ is 95.1 dB(A) (Table 4), which is only 0.5 dB(A) higher than the $L_{\rm eqm}$ of the inspection watches. The measured $L_{\rm eqm}$ appears to be one dB higher than $L_{\bar{A}}$ of the three lower decks, which is 94 dB(A). This is mainly caused by the high $L_{\rm eqm}$ occurring during maintenance work with respect to the auxiliary diesel engines when the averaged value of $L_{\rm eqm}$ appears to be 99 dB(A) (Table 9).

From Table 1 it appears that the $L_{\bar{A}}$ obtained from the sound levels measured near the auxiliary engines is about 97.5 dB(A), which is only one dB lower than L_{egg} (unrounded 98.5 dB(A)).

During the majority of the maintenance work the average value of $L_{\rm eq_m}$ is 94 dB(A) (Table 9) which equals $L_{\bar{A}}$ of the three lower decks.

For the harbour condition (Table 5) the $L_{\rm eq_m}$ of 91.6 dB(A) is 0.5 dB higher than the average value of the sound levels at the three lower decks.

So it may be concluded that aboard the ship con-

Table 7. The measured and calculated $L_{\rm eqm}$ for the inspection watches

round	L_{eq_m} measured (see table 3)	L_{eq_m} calculated using routes and $L_{\overline{A}}$ per area of 1.5×1.5 m	$L_{\rm eq_m}$ calculated using exposure time per deck and $L_{\widetilde{A}}$ per deck (see table 6)
по.	(see table 3)		(see table 6)
1	94.8	92.3	94
2	92.3	91.8	92.9
3	95.6	93.7	94.1
4	96.8	93.1	93.9
5	_	94.0	93.3
6	_	93.4	93.5
7	96.3	92.7	93.9
8	94.8	93.2	93.6
9	95.0	94.1	93.4
10	96.0	92.4	94.3
11	98.4	93.9	94.3
12	94.4	92.9	94.0
13	94.7	94.3	94.3
14	94.4	96.7	94.4
15	95.1	93.2	93.8
16	94.9	93.8	93.9
17	94.6	93.7	94.1
18	_	92.1	93.9
19	92.6	93.0	93.6
20	, · · · ·	94.1	94.1
21	95.3	93.7	93.5
22	95.2	95.7	94.6
23	93.4	92.3	93.7
24	96.7	94.2	94.1
25	95.4	93.4	93.7
26	94.5	94.5	94.4
27	94.8	93.7	93.5
28	95.9	94.8	94.3
29	92.8	94.1	93.8
30	93.9	94.1	94.1
31	92.4	92.4	92.9
32	90.5	94.0	94.3
33	90.7	93.8	93.8
n =	29	33	33
$\bar{x} =$	94.6	93.6	93.9
s =	1.7	1.0	0.4

cerned the measured $L_{\rm eqm}$ agree with the averages of the levels $L_{\bar{A}}$ measured at the three lower decks in the engine room except with respect to the maintenance work concerning the auxiliary diesel engines where the sound levels in the vicinity of these engines are responsible for the $L_{\rm eq}$.

Table 8. The measured and calculated L_{eq_8} for the inspection watches

round no.	$L_{ m eq}_{ m 8}$ measured	L_{eq_8} calculated using $L_{\overline{A}}$ per area	L_{eq_8} calculated using $L_{\bar{A}}$ averaged per deck
1	82.7	80.6	82.0
2 3	83.3	82.9	83.8
3	88.5	86.7	87.1
4	84.1	81.3	81.9
7	83.1	79.8	81.2
8	82.5	81.4	81.5
9	82.5	81.8	81.3
10	88.3	84.6	86.7
11	85.8	82.6	82.4
12	86.6	84.2	85.2
13	82.3	82.0	82.0
14	81.5	83.3	81.5
15	87.7	85.9	86.5
16	83.0	82.1	82.2
17	86.7	85.8	86.2
19	83.9	84.3	84.8
21	85.5	84.1	83.9
22	83.1	83.9	83.0
23	84.6	83.7	84.9
24	83.1	81.2	81.1
25	88.1	86.2	86.5
26	82.3	82.3	82.2
27	86.6	85.6	85.4
28	83.0	82.1	81.8
29	84.5	85.8	85.5
30	81.0	81.1	81.1
31	83.5	83.5	84.0
32	79.6	82.0	82.2
33	78.5	80.3	80.3
n =	29		
$\bar{x} =$	84.0	83.1	83.4
s =	2.5	1.9	2.1

Table 9. Summary of the averaged values of the results of the noise dose measurements. The $L_{\rm eq}$ and their standard deviation s levels (in dB(A)) are given using the measuring time ($L_{\rm eq}_{\rm m}$) or 8-hours ($L_{\rm eq}_{\rm g}$) as the integration time

_								
measuring conditions		number of measurements	$L_{ m eq}$	_m S	$L_{ m eq}$	$L_{ m eq}_{8}$ s		
1.	sailing, inspection watches	29	95	1.7	84	2.5		
2.	sailing, maintenance watches	62	95	3.6	91	4.1		
2a.	from 2, maintenance of auxiliary diesel engines only	16	99	1.0	95	1.2		
2b.	other maintenance watches than 2a	46	94	3.4	90	4.0		
3.	in harbour, watches and maintenance	22	92	2.6	87	3.6		

Table 10. Comparison between the L_{eq} obtained by measurement using noise monitors and by calculation using measured sound levels and exposure times

		$L_{^{\mathbf{eq}}_{8}}$	L_{eq_8}	calculation based on					
measuring conditions		measured (dB(A))	calculated (dB(A))	L_{A_i}	during	$t_i(min)$	table no.		
1.	sailing, inspection watches	84	83/83 84	94 80	many data (decks 1-3) (control room)	42 210-42 = 168	8 1, 6 1, 3		
2.	sailing, maintenance watches	91	90	94	(decks 1-3)	211	1, 4		
2a.	from 2, maintenance of auxiliary diesel engines only	95	94	97	(deck 1, near aux. diesel eng.)	207	1, 4		
3.	in harbour, watches and maintenance	87	88	91	(decks 1-3)	228	2, 5		

7.2

To evaluate the noise exposure of the engineers with respect to the hearing impairment noise limit, $L_{\rm eq}$ based on an integration time of 8 hours, $L_{\rm eqs}$, is used.

The values of L_{eqs} , calculated by using the measured $L_{\rm eg_m}$ and the exposure times, are given in the Tables 3, 5 and 8. This incorporates that when calculating L_{eqs} it is supposed that within the total time of 8 hours only exposure to sound in the engine room and control room exists. Moreover, L_{eq8} is calculated using the exposure during a 4-hour watch which includes that the L_{eqs} given in the tables do not directly give an impression about the total noise exposure per week-day, which will be discussed in the next paragraph. In the Figs. 1–3 the distribution of the levels is illustrated. Only the L_{eqs} measured during inspection watches (Fig. 1) and during maintenance work at the auxiliary diesel engines tend to a normal distribution of the levels. However, the amount of data is too small in fact to arrive at conclusions in this respect.

The L_{eq_8} shows in general a higher standard deviation than the L_{eq_m} which is caused by the deviations of data of the exposure times.

The averaged value of $L_{\rm eqs}$ of the inspection watches, 84 dB(A), appears to be 7 dB(A) lower than the $L_{\rm eqs}$ of the maintenance watches which is due to the short exposure time during the rounds through the engine room. The $L_{\rm eqs}$ calculated by using the sound levels and exposure times are given in the Tables 8 and 10. The calculated levels are in good agreement with the measured levels if for the calculation the right assumption about the levels to be used is made and the average exposure times, given in table 10 are used. The assumptions are

- 1. the mean-square space averaged A-weighted sound pressure level $L_{\bar{A}}$ may be used
- 2. the $L_{\bar{A}}$ of the three lower levels in the engine room determines $L_{\rm eqs}$ during sailing and the $L_{\bar{A}}$ of the floor during harbour conditions
- 3. when maintenace work is executed the levels in the

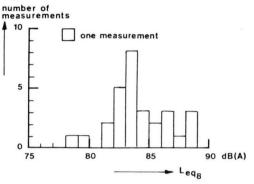


Fig. 1. Distribution of the equivalent sound levels (reference time: 8 hours) measured during the normal four-hour watches at service speed condition.

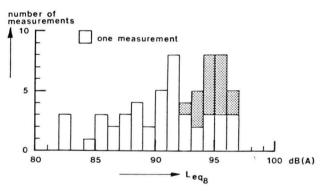


Fig. 2. Distribution of the equivalent sound levels (reference time: 8 hours) measured during the four-hour maintenance watches spent in the engine room. The shadowed area refers to measurements during watches during which auxiliary diesel engines were repaired.

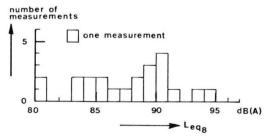


Fig. 3. Distribution of the equivalent sound levels (reference time: 8 hours) measured during the watches at harbour conditions

vicinity of the engine(s) involved can be used to calculate L_4 .

Because the $L_{\rm eqs}$ based on the measured data may be considered as a sample of the total collection of occurring $L_{\rm eqs}$ it can be stated that the average value of these measured $L_{\rm eqs}$ is a good rating for the real $L_{\rm eqs}$ with inaccuracy of ± 1 dB (inspection and maintenace, Tabels 3 and 4) or of ± 1.5 dB (harbour, Tables 5) within a confidence range of 95%.

Calculation of L_{eqs} increases this inaccuracy only slightly.

7.3

To assess the noise exposure per week for an engineer aboard the m.v. "Trident Amsterdam" the distribution of the two types of watches during a week has to be considered. Aboard the ship an engineer keeps two four-hour watches a day and in a period of three days two inspection watches and four maintenance watches. This scheme is continued for long periods, seven days a week. So it is obvious to consider the $L_{\rm eq}$ for a period of six 4-hour watches, giving 24 hours exposure-time. To obtain $L_{\rm eq_{24}}$ for one watch 5 dB has to be subtracted from the respective $L_{\rm eq_8}$:

$$L_{\text{eg}_{34}} = L_{\text{eg}_8} - 10 \log 24/8 = L_{\text{eg}_8} - 5 \text{ dB}$$

The resulting $L_{eq_{24}}$ of six 4-hour watches can now be derived by addition of the six $L_{eq_{24}}$ following the power law:

$$L_{\text{tot}} = 10 \log (10^{0.1L_1} + 10^{0.1L_2} ... + 10^{0.1L_6})$$

For two inspection- and four maintenance watches, using the data of table 10 from which 5 dB are subtracted, the resulting $L_{\rm eq}$ becomes:

$$L_{\text{eq}_{24}} = 10\log(10^{7.9} + 10^{7.9} + 10^{8.6} +$$

When in all periods of 24 hours this $L_{\rm eq}$ occur the $L_{\rm eq56}$ in a working week of 56 hours is 92.5 dB(A). The contributions of the inspection and the maintenance watches to this level are 82 and 92 dB(A) respectively.

In [2] a working week of 40 hours is used. It is not known at the moment if the risk of hearing impairment increases when the number of working hours per week increases. Supposing the equal energy concept, on which [2] is based, is also valid for periods with more than 40 hours, the $L_{\rm eq_{40}}$ for a 40-hour week would be 94 dB(A).

In the introduction it is mentioned that, to be sure that the limit of 90 dB(A) at the protected ear is not surpassed, the level in the engine room would not exceed 98 dB. The $L_{\rm eq40}$ is 4 dB lower which involves that

it is unlikely that the sound level at the ears, when using earmuffs would exceed 86 dB(A). From some experiments carried out aboard it appeared that inside the earmuffs the sound level was lower than 80 dB(A). So, when using earmuffs, the engineers aboard the m.v. "Trident Amsterdam" have a low risk of hearing impairment.

8 Conclusions

- 1. The direct measured and calculated equivalent continuous sound levels $L_{\rm eq}$, being the continuous levels which would result in the same amount of sound energy as it would be in the case for the varying levels, proved to be in good agreement.
- 2. For this particular ship the level of the mean-square space averaged sound pressure \bar{p}^2 measured at the three lowest levels in the engine room appears to offer a reliable base for the calculation of $L_{\rm eq}$.
- 3. The method by which the data is gathered needs no further improvement. The necessity of having a person aboard whose task is to coach the engineers with respect to the use of the noise monitors and to administrate carefully the exposure times appeared clearly during the interpretation of the results.
- 4. The L_{eq} for a 56-hours week appears to be 92.5 dB(A). This level is composed of a contribution of 82 dB(A) caused by the exposure to noise during the inspection watches and by a contribution of 92 dB(A) caused by maintenace work.

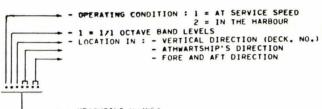
9 Acknowledgement

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References

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- ISO-Recommendation R1999: Assessment of occupational noise exposure for hearing conservation purposes.

Table 1. Survey of sound pressure level measurements



	- MEAS	SU⊇ II	NG :10:	13E+	2							
	SOUND-N		CENTO				05.0		 E BA	NDS	IN H7	
MEASUR-	LEVEL-N	IUM-	CENTRE									
NUMBER	.V.	BER	31.5	63	125	250	500	1K	2K	4K	8K	
1110125	88	84	99	98	90	89	87	82	78	71	73	
1110130	85	80	95	98	89	86	82	80	76	70	72	
1110135	85	80	101	96	89	85	83	80	77	71	68	
1110140	85 92	89	91	93 87	88	89	83 91	80	77 85	72 76	68 72	
1110145	91	87	92	95	87	89	89	86	85	77	73	
1110247	93	89	90	92	90	91	91	88	86	79	75	
1110249	94	91	93	95	40	92	93	89	87	80	77	
1110250	94	91	95	93 93	91	93	93	89 90	97 87	80	77 77	
1110251 1110252	96	94	93	92	90	95	96	91	88	81	78	
1110253	95	93	92	92	91	94	95	91	89	82	78	
1110254	95	92	93	95	90	94	94	91	88	81	78	
1110255	96	92	93	97	88	95	94	91	88	81	78 79	
1110256	96 94	92	92 91	94	87	94	94 93	92	88	82	77	
1110258 1110345	92	99	71	96	88	89	91	87	84	77	73	
1110447	94	91	92	95	90	91	93	89	87	81	78	
1110449	98	94	91	94	91	93	96	92	92	86	84	
1110450	99	96	93	94	91	92	98	94	93	87 87	84	
1110451	100	98	91	93	92	93	100	93	90	83	31	
1110455	94	94	90	91	e9	94	96	93	91	83	81	
1110456	97	94	93	91	91	93	95	93	91	83	81	
1110457	97	94	91	92	41	93	96	93	90	83	82	
1110458	96	93	92	95	89	93 93	95 93	91 90	87	83 81	81 78	
1110548 1110550	98	96	95	93	91	95	98	94	90	84	80	
1110552	99	96	93	93	90	94	97	96	91	85	83	
1110554	97	93	94	93	91	93	94	93	90	84	81	
1110555	97	93	94	94	90	94	95 97	93	91	84 87	81 83	
1110556	99	96 96	95 95	93	90	94	98	93	93	87	84	
1110557	97	94	94	93	88	94	94	92	92	86	87	
1110660	94	91	95	94	91	94	93	90	86	79	77	
1111158	94	90	89	89	89	94	92	89	87	79	75	
1111245	90	85 89	92 92	98	87 90	88	88 89	85	83 87	75 77	71 73	
1111248	92	88	94	95	91	91	89	87	86	77	72	
1111250	95	94	96	93	90	90	89	87	92	77	72	
1111251	94	92	96	94	90	91	89	87	90	78	72	
1111252	93	91	95	93	89	91	90	87 87	89 91	78 78	72 72	
1111253 1111254	94 94	93 92	94	91	91	90	91 91	88	90	78	71	
1111255	93	90	93	92	90	90	91	87	88	78	71	
1111256	93	90	92	92	89	90	90	88	88	78	72	
1111258	94	90	91	9u 89	89	92	92	89	88	79 77	75 72	
1111347 1111355	92	88	90	90	87	91	90	87	86	79	74	
1111446	89	85	95	89	86	87	88	84	83	74	69	
1111447	91	87	93	89	89	88	89	86	85	77	72	
1111450	91 93	98	92 91	90	86	90	88	86	86 90	76 77	70 70	
1111452 1111454	92	88	93	86	86	89	89	87	86	78	72	
1111457	93	90	88	91	88	91	90	88	88	80	75	
1111458	93	89	92	57	87	90	91	88	86	80	75	
1111549	91	88	94	90	87	89	88	86	86 89	76 79	72 75	
1120148	93	91	93 88	94	88	90	90 91	88	86	79	74	
1120158	93	89	88	92	88	91	91	89	87	79	74	
1120249	93	90	90	90	89	91	91	87	88	81	81	
1120250	93	89	90	90	90	92	91	86 89	87 88	82 84	80 84	
1120251	95 95	90	92 92	92	90	92 92	92	90	88	82	81	
1120252	95	91	92	89	91	92	93	90	88	81	79	
1120254	95	90	91	91	90	93	92	90	88	82	80	
1120255	92	89	90	87	89	92	91	87	84	77	74	
1120256	94	90	91	87	89	93	92	89	87 87	80	78 76	
1120257 1120258	94	90	89	90	58	92 91	90	89	88	79	75	
1120348	03	79	89	84	83	82	82	78	74	65	61	
1120357	93	89	89	92	88	91	91	89	87	79	77	
1120451	81	77	88	83	82	80	79	77	73	63	61	
1120453	80 79	75 75	84	82	79 78	80 79	78 77	75 75	72 71	61	58 56	
1120455 1120457	79	74	82	83	77	80	77	74	72	61	58	
1120547	84	80	87	88	85	83	83	79	75	65	60	
1120549	86	82	91	88	B7	87	85	81	77	68	63	

No.	Table 1.	(continu	ed)									
												IN HZ
										2K		8K
1120555												
1120649												
				93	89	89	89	86	82	78	69	65
1121254	1121157	94	92	90	94	89	91					
1121254									89	94	82	74
1121556												
1121446	1121256	94	92	92	94	89	93	90	89	90	80	75
			91						87	89	78	69
1121455												
12145a	1121455	95	94	94	94	87	90	89	88	92	80	73
121556		94	93						87	91	77	70
12 558	1121550											
1130148	1121558	94	93	93	91	85	89	89	87	91	78	72
1130157												
1130250	1130157											
130262	1130250	91	89	89	89	89	88	88	88	85	77	73
130255												
130255	1130253	93	91	99	91	89	88	89				
1130258						88						
1130348												
130454	1130348	90	87	91	89	86	87	87	86	85	76	72
130456												
130548	1130456											
130654		85	82	90	82	81	84	83	82	77	70	66
130558												
130750	1130658	87	84	83	86	85	86	85	84	80	72	67
130756				91	82				79	73	66	63
131150	1130752											
131156	1131149	90	87	93	92	90	88	87	87	84	75	72
1131158												
131248	1131157											
1131251	1131248	92	91	92	92	87	88	86	87	89	78	73
1131255												
131257	1131255											
1131352	1131257	92	89	92	92	89	88	90	88	87	78	72
1131354												
1131448												
131458	1131448	87	84	90	86	85	84	83	83	82	74	67
1131548												
1131554 77 73 83 80 80 78 75 72 71 62 55 1131748 82 78 86 85 82 79 78 77 76 69 64 1131750 82 79 88 83 82 80 76 77 77 66 96 1131753 73 69 93 77 76 75 70 69 66 57 50 1131758 76 71 92 79 77 76 73 71 69 60 54 1131758 76 71 92 79 77 76 73 71 69 60 54 1131758 1140348 88 85 90 92 86 84 85 85 82 73 70 1150250 91 88 91 91 87 87 88 83 85 85 87 37 70 1150250 91 88 91 91 84 81 83 82 80 70 68 1150348 86 82 96 91 84 81 83 82 80 70 68 1150351 91 88 93 93 88 86 88 87 88 86 76 73 1150250 1160251 87 83 93 88 87 88 85 85 87 77 77 1160251 88 85 90 92 86 84 82 82 82 77 72 1160253 89 86 91 88 85 90 89 89 85 85 85 81 73 70 1160253 89 86 91 88 85 90 89 89 85 85 85 81 73 70 1160253 89 86 91 88 85 84 85 85 85 81 73 70 1160255 88 85 91 92 86 84 85 85 86 84 75 71 1160251 87 83 93 88 87 85 83 83 81 71 72 1160253 88 86 91 98 88 85 84 85 85 86 84 73 70 1161250 86 82 90 86 88 85 84 85 85 87 77 22 77 1160251 87 83 93 88 87 85 83 83 81 71 72 1160253 89 86 91 88 85 84 85 85 86 84 73 70 1161250 86 82 90 86 88 83 83 82 79 70 70 67 1161251 88 84 91 90 87 82 82 82 81 77 69 69 1161155 89 86 87 89 88 85 85 85 86 84 73 69 1161155 89 86 87 89 88 85 85 85 86 84 73 69 1161155 88 84 93 93 93 88 88 88 88 88 88 88 88 88 88 88 88 88	1131548	85	83	87	87	82	81	79			72	67
1131750			73				78	75	72	71	62	55
1131753												
1131758	1131753	73	69	93	74	76	75	70	69	66	57	50
1150148	1131758	78	75	82	77	77	77	75	74	73	63	56
1150250												
1150351 91 88 93 93 88 86 87 88 86 76 73 1151248 89 86 95 86 84 82 85 86 84 75 71 1160152 88 85 90 89 89 85 85 85 81 73 70 1160250 86 83 95 89 86 82 82 82 79 72 77 1160251 87 83 93 88 87 85 83 83 81 71 72 1160253 89 86 91 88 85 84 85 85 84 73 70 1160255 88 85 91 92 86 84 85 85 82 72 69 1161150 85 81 91 90 87 82 82 81 77 69 69 1161155 89 86 87 89 88 85 84 85 85 85 85 77 69 69 1161251 88 84 93 89 87 82 82 81 77 69 69 1161251 88 84 93 89 87 88 86 84 79 70 67 1160251 86 82 87 91 88 85 84 85 85 85 85 85 85 85 85 85 85 85 85 85	1150250	91	88	91	91	87	87	86	88	84	76	73
1151248 89 86 95 80 84 82 85 86 84 75 71 1160250 86 83 95 69 89 85 85 81 73 70 1160250 86 83 93 88 87 85 83 81 71 72 77 1160253 89 86 91 88 85 84 85 85 81 71 72 1160253 89 86 91 88 85 84 85 85 81 71 72 1160255 88 85 91 92 86 84 85 85 82 72 69 1161150 85 81 91 90 87 82 82 81 77 69 69 1161250 86 82 90 86 88 83 82 79 70		91	88	93	93		88	87	88	86	76	73
1160250 86 83 95 89 86 82 82 79 72 77 1160251 87 83 93 88 87 85 83 83 81 71 72 1160255 88 85 91 92 86 84 85 85 82 72 69 1161250 86 81 91 90 87 82 82 81 77 69 69 1161250 86 82 90 86 88 83 82 79 70 67 1161251 88 86 93 89 87 88 86 84 79 70 67 1170249 84 80 93 93 88 84 83 82 82 79 70 67 1170251 86 82 90 93 88 84 83 80 70												
1160253 89 86 91 88 85 84 85 85 84 73 70 1160255 88 85 91 92 86 84 85 85 82 72 69 1161150 85 81 91 90 86 84 85 85 82 72 69 1161250 86 82 90 86 88 83 83 82 79 70 67 1161251 86 82 87 91 88 86 84 79 71 67 1170152 86 82 87 91 88 86 84 79 71 68 1170249 84 80 93 93 87 81 80 77 70 68 1170253 87 83 88 87 86 83 84 83 80 70 67	1160250	86	83	95	89	86	82	82	82	79	72	77
1160255 88 85 91 92 86 84 85 85 82 72 69 1161150 85 81 91 90 87 82 82 81 77 69 69 1161250 86 82 90 86 88 83 83 82 79 70 67 1161251 88 84 93 89 87 88 86 84 79 70 67 1170249 84 80 93 93 87 81 81 80 77 69 66 1170251 86 82 90 93 88 84 83 77 70 67 1170251 86 83 90 93 88 84 84 83 77 70 68 1170253 87 83 88 87 88 84 83 80 70												
1161155 89 86 87 89 88 85 85 84 73 69 1161250 86 82 90 86 88 83 82 79 70 67 1161251 88 64 93 89 87 88 86 84 79 71 68 1170152 86 82 87 91 88 83 82 82 79 69 66 1170249 84 80 93 93 87 81 81 80 77 69 66 1170253 86 83 90 93 88 84 83 80 70 67 1171149 84 81 87 88 85 81 82 81 77 69 66 1171151 85 82 89 87 82 82 82 79 69 66	1160255	88	85	91	92	86	84	85	85	82	72	69
1161250 86 82 90 86 88 83 82 79 70 67 1161251 88 64 93 89 87 88 86 84 79 71 68 1170152 86 82 87 91 68 83 82 82 79 69 66 1170251 86 83 90 93 88 84 84 83 77 70 68 1170253 87 83 88 87 86 83 84 84 83 60 70 67 1171149 84 81 87 88 85 81 82 79 69 66 1171151 85 82 86 89 87 82 82 79 69 66 1171153 86 83 86 89 87 82 82 79 69 66 1171254 87 84 91 90 82 83 84	1161155	89	86	87	89	88	85		85	84	73	
1170152												
1170251 86 83 90 93 88 84 84 83 77 70 68 1170253 87 83 88 87 86 83 84 83 80 70 67 1171149 84 81 87 88 85 81 82 81 77 69 66 1171151 85 82 86 89 87 82 82 82 79 69 66 1171151 85 81 86 88 88 83 83 83 79 70 67 1171251 85 81 86 88 88 83 82 81 79 68 65 1171254 87 84 91 90 89 82 83 84 79 70 66 1180151 87 89 94 100 99 85 81 81 77 69 63 1180152 84 80 94 96 90 84 81 80 76 69 63 1180153 85 81 96 95 90 87 79 80 77 69 63 1180154 85 82 96 97 93 85 80 80 77 69 63	1170152	86	82	87	91	88	83	82	82	79	69	66
1170253	1170251	86	83	90	93	88	84		83			
1171151 85 82 86 89 87 82 82 82 79 69 66 1171153 86 83 86 92 89 83 83 83 79 70 67 1171251 85 81 86 88 88 83 82 81 79 68 65 1171254 87 84 91 90 89 82 83 84 79 70 66 1180151 87 89 94 100 99 85 81 81 77 69 63 1180152 84 80 94 96 90 84 81 80 76 69 63 1180153 85 81 86 95 97 93 85 80 80 77 69 63							83	84	83	80	70	67
1171251 85 81 86 88 88 83 82 81 79 68 65 1171254 87 84 91 90 89 82 83 84 79 70 66 1180151 87 89 94 100 99 85 81 81 77 69 63 1180152 84 80 94 96 90 84 81 80 76 69 63 1180153 85 81 96 95 90 87 79 80 77 69 63 1180154 85 82 96 97 93 85 80 80 77 69 63	1171151	85	82	86	89	87	82	82	82	79	69	66
1171254 87 84 91 90 89 82 83 84 79 70 66 1180151 87 89 94 100 99 85 81 81 77 69 63 1180152 84 80 94 96 90 84 81 80 76 69 63 1180153 85 81 96 95 90 87 79 80 77 69 63 1180154 85 82 96 97 93 85 80 80 77 69 63	1171251											
1180152 84 80 94 96 90 84 81 80 76 69 63 1180153 85 81 96 95 90 87 79 80 77 69 63 1180154 85 82 96 97 93 85 80 80 77 69 63		87	84	91	90	89	82	83	84	79	70	66
1180154 85 82 96 97 93 85 80 80 77 69 63	1180152	84	80	94	96	90	84	81	80	76	69	63
	1180154	85	82	96	97	93			80	77		63
	1181151	85	82	94	96	93	85	81	80	76	68	

Table 1. (continued)

											 IN 47
MEASUR-	SOUND-N	UM							 2K		
NUMBER			1.5	63		250		1K		4K	8K
1181154	84 84	80	96 97	90 96	90	84 82	79 79	80 79	77 77	70 69	63 63
1181251	86 77	86	95 85	101	97 75	85 78	80 75	80 71	76 65	68 57	61 50
2110125 2110130	79	78	82	97	79	76	79	74	69	61	56
2110140 2110146	83 92	90	82	79 88	80 87	82 88	83 92	78 86	73 84	67 79	63 76
2110247	94 97	91 93	91	87 91	88	90	93 95	89 91	86 90	81 85	78 84
2110250	98	94	92	93	86	92	96	93	91	86	83
2110251 2110252	98 98	95 94	93 92	95 96	90	93 92	97 96	94 93	91 91	85 85	81
2110254 2110256	95 92	92	90	99	86 85	92 89	94	90 88	87 83	80 77	76 72
2110345	92 96	91	85	83 94	86 91	89 93	93 95	87 91	83 90	77 85	74 82
2110450	99	96	89	100	92	94	98	94	93	87	84
2110451 2110453	99 95	97 92	88 85	97 92	91 89	93 90	99	94 91	93 87	85 80	83 78
2110455 2110457	90 89	87 86	83	86 91	85	87 87	90	86 85	82 81	75 74	70 69
2110458	88 94	85 91	84	87 89	82	84 92	88 93	84 89	79 86	72 80	67 76
2110548 2110550	97	94	94	92	94	95	96	93	90	82	80
2110552 2110555	98 89	96 85	92 87	92	89	95 87	98 88	94 84	90 81	83 74	81 69
2110557 2111158	89 88	85 85	87 89	93 92	83 85	87 86	88	84 83	81 79	74 73	69 67
2111245	90	86	92	85	85	89	89	85	82	76	73
2111249 2111251	88 87	84	90	87 85	85 88	89 86	87 86	83 82	79 78	74 73	71 67
2111253	86 86	82 82	90	91	87	36 35	85 85	81 82	77 77	72 72	66 65
2111258	87	83	85 83	90 87	89	87 91	86 87	82 85	78 80	72 75	65 72
2111347 2111355	86	82	84	83	84	86	85	82	78	73	67
2111446 2111450	89 87	85 83	86 87	87 85	85 85	87 85	88 86	84 82	80 78	74 72	70 67
2111452 2111454	87 87	83	90	89	82	85 86	86 86	83 81	80	75 74	69 67
2111457	86	82	84	88	83	86	85	81	77 77	73	67
2111458 2120157	85 87	81 84	87 82	87 89	83 82	85 85	84 87	83	79	72 72	65 66
2120249 2120251	91 91	89 89	89	84	85 87	89 89	91 91	85 86	81 83	75 77	70 72
2120253	92 90	89 86	88	88	87	89 86	91 89	88 85	84 82	77 75	72 68
2120258	88	85	81	88	83	86	88	84 74	80 69	73	67
2120453 2120455	78 78	75 74	76 81	77 81	77 77	78 77	78 77	74	68	57 56	52 50
2120457 2120547	78 89	74 86	79 87	76 91	78 86	78 89	77 89	73 83	68 79	56 72	49 67
2120549 2120555	89 86	87 83	83 93	88 95	87 89	89 89	90 86	83 80	79 75	72 63	68 57
2120559	83	80	90	87	81	84	83	78	70	60	54
2120649 2120651	88 91	85 88	90	87 87	92	89 94	90	84	78 80	70 71	65 65
2121158 2121256	87 84	83 80	82	87 86	81	85 84	86	80	78 75	71 70	65 64
2121358	85 86	81 83	83 86	92 89	80	83 84	84 86	81	76 76	70 71	65 64
2121453	85	81	83	82	83	84	84	80	76	71	64
2121455	84 86	83	82	86	80	85	86	80 81	78	73	65
2130249 2130251	86 85	82 81	87 87	88	85 85	85 86	85 84	81	76 77	70 69	64
2130254 2130256	83 83	79 79	83	90	83	83	82 82	78 78	74 75	67 67	61
2130258	85	82	85	88	81	82	85	81	76	69	62
2130348 2130349	84 86	81	86 89	86 87	84	83 85	84	80	75 77	69 70	64
2130454 2130654	84	80 78	84	89	80	82	83 81	80 76	76 71	69 63	62 56
2130558 2130747	82 78	78 74	80 95	79 83	80	81 79	81	78 74	72 68	64	56 56
2130750	82	78	86	53	81	63	81	77	72	65	60
2130752 2130756	83 81	80 78	94	89	85	86	82 81	77 77	72 72	67 64	68 56
2131157 2131158	83 85	81	83	88 87	82	82	83	79 81	74 76	67	61
2131248	86 84	81	88 91	91 95	85	87 85	84 82	81	77 75	70 69	66
2131250 2131251	95	81	32	85	86	86	83	81	75	67	60
2131255 2131257	84	78 81	88	85 85	82	81	80 84	78 79	73 75	66 68	59 60
2131353 2131354	88 81	85 77	96	95	88	85 82	87 80	85 77	79 72	71 65	65 59
2131448	82	78	89	81	82	81 79	81	77 75	73 71	67 65	63 62
2131549 2131750	77	75 73	34 35	79	78	79	75	73	68	62	59
2140348 2150148	84 82	80 78	92	94	80	84	83	79 78	74 73	67 67	62 61
2150348	79 84	75	92	89	83 88	78 84	78 83	75 79	70 75	62 67	57 63
2151248	82	78	93	92	80	82	80	78 77	73	66	61
2160152 2160250	81	77	86	92	84	81	80	76	72	66	60 64
2160251 2160253	85 82	82 78	8 7	87 85	88 84	86 82	85 81	79 78	74 74	70 67	68 62
2160255 2161155	81 82	77 78	84	91	81	79 80	79 80	77 78	72 73	66 66	60
	6								-		

Table 1. (continued)

MEASIIR-	SOUND-	NR-	CENTR	E FF	REQUE	NCY	OF (CTAV	E BA	NDS	IN HZ
ING	LEVEL-										
MINABER	• 4 •	958	31.5	63	125	250	500	1 K	2K	4K	8K
2161251	84	79		88	86	85	82	79	74	68	63
2170152	82	78	83	93	88	32	81	77	73	67	61
2170249	80	76	85	90	86	79	79	74	69	64	61
2170251	A1	77	36	91	84	32	80	76	71	65	60
2170253	80	76	85	90	85	82	79	75	71	64	59
2171149	85	76	92	88	83	80	79	76	71	64	58
2171151	82	78	83	91	86	81	80	78	74	67	62
2171153	81	76	84	93	85	80	79	76	72	66	60
2171251	81	77	85	89	86	81	80	77	72	64	59
2171254	81	76	85	86	85	80	79	76	72	65	58

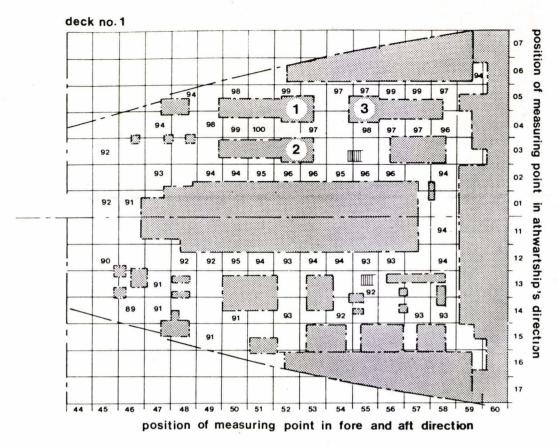


Fig. 1. View on deck no. 1 (floor). The sound levels-A measured at the several locations are given in the concerned rectangular

Operational condition: at service speed.

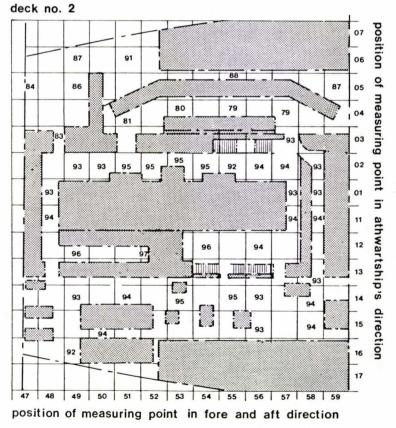


Fig. 2. View on deck no. 2 (2nd Tweendeck). The sound levels-A measured at the several locations are given in the concerned rectangular sections. Operational condition: at service speed.

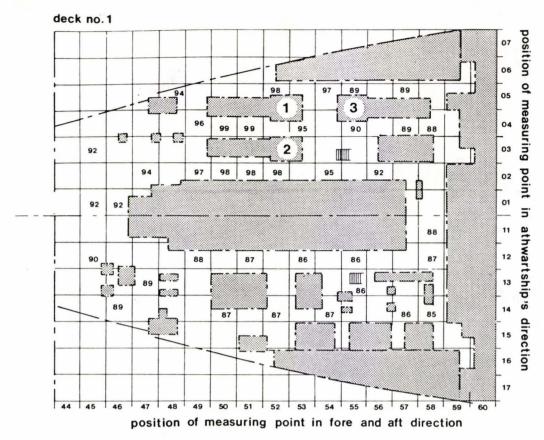


Fig. 5. View on deck no. 1 (floor). The sound levels-A measured at the several locations are given in the concerned rectangular sections.
Operational condition: in the harbour.

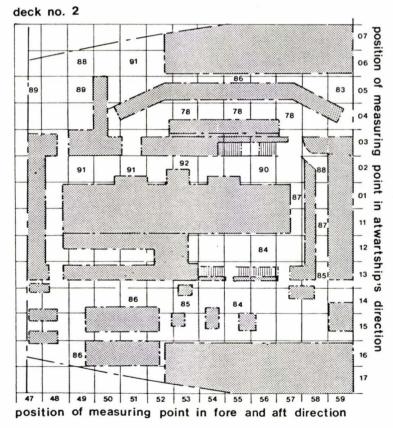


Fig. 6. View on deck no. 2 (2nd Tweendeck). The sound levels-A measured at the several locations are given in the concerned rectangular sections.

Operational condition: in the harbour.



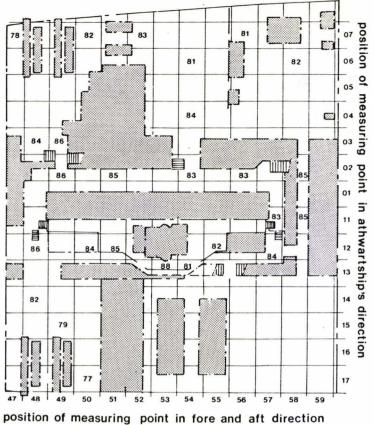


Fig. 7. View on deck no. 3 (1st Tweendeck). The sound levels-A measured at the several locations are given in the concerned rectangular sections.

Operational condition: in the harbour.

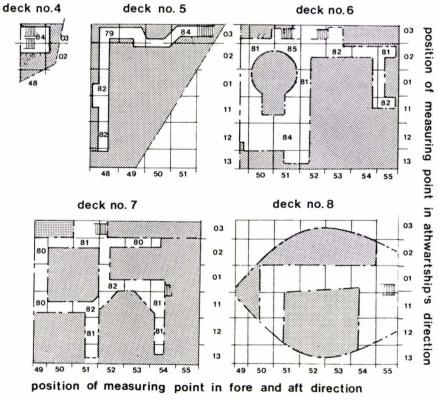


Fig. 8. View on decks no. 4-8 (A-E deck). The sound levels-A measured at the several locations are given in the concerned rectangular sections.
Operational condition: in the harbour.

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